OPTIMIZATION OF THE EFFLUENT TREATMENT SYSTEM (ANAEROBIC/AEROBIC) FOR RUBBER INDUSTRY BY KINETIC MODELING

The state of the s

Indika Upuli Hettiarachchi

This thesis was submitted to the Department of Chemical & Process Engineering of the University of Moratuwa in partial fulfillment of the requirements for the Degree of M.Sc. in Polymer Technology (2000/2001).

Department of Chemical & Process Engineering
University of Moratuwa

Sri Lanka.

December, 2003.

um Thesis coll.

niversity of Moratuwa

79629

Contents

	Page number	
Declaration	I	
Abstract	II, III, IV	
Acknowledgement	V	
List of tables, figures, annexures	VI,VII,VIII,IX	
List of symbols & acronyms	X, XI	
Chapter 1: Introduction		
1.1 The natural rubber industry in Sri Lanka		1
1.2 Environmental problems caused by the natural rubber indu	stry in Sri Lanka	2
1.3 Environmental pollution control in rubber processing indus	stry	3
1.4 Scope of the study		4
1.5 Objectives		5
Chapter 2: Literature Review		
2.1 Rubber effluent characteristics		6
2.1.1 Concentrated latex production process		7
2.1.1.1 Production process		7
2.1.1.2 In-plant pollution control		11
2.1.2 Processing of latex into crepe rubber		11
2.1.2.1 Production processes		11
2.1.2.2 In-plant pollution control		15
	*	
2.2 Treatment of wastewater		18
2.2.1 Classification of wastewater treatment methods		- 18 °
2.2.1.1 Physical treatment methods		18
2.2.1.2 Chemical treatment methods		18
2.2.1.3 Biological treatment methods		19

2.3 Biological treatment processes	19
2.4 The RRI based cost effective biological treatment process	20
2.4.1 The mechanism of anaerobic digestion	24
2.4.2 Biological processes in the aerobic tanks	26
2.4.3 Factors depending on the growth of bacteria	27
2.4.3.1 The pH	27 .
2.4.3.2 The alkalinity	28
2.4.3.3 The temperature	28
2.4.3.4 Nutrients	28
2.5 Biological treatment for industrial wastewater	29
2.5.1 Nutrient & growth factor requirements	30
2.5.2 Kinetics of biological growth	30
2.5.2.1 Cell growth	31
2.5.2.1.1 Cell growth & substrate utilization	31
2.5.2.1.2 Effects of endogenous metabolism	31
2.5.2.1.3 Effects of temperature	32
2.6 Activated-sludge process	34
2.6.1 Process design	35
2.6.2 Process description	35
2.6.3 Process microbiology	36
2.6.4 Process analysis	37
2.6.5 Process design & control relationships	39
2.6.5.1 Sludge production	40
2.6.5.2 Oxygen requirements & transfer	40
2.6.5.3 Nutrient requirements	41
2.6.5.4 Effluent characteristics	41
2.6.6 Process control	41

.

2.6.6.1 Dissolved- oxygen control	42
2.6.6.2 Return activated-sludge control	43
2.6.6.3 Sludge wasting	44
2.6.6.4 Oxygen-uptake rates	45
Chapter 3: Materials & Methods	
3.1 The experimental apparatus	46
3.1.1 Measurement of BOD using BOD apparatus	47
3.1.2 The VSS test	48
3.2 Operating conditions of the full-scale activated-sludge process	48
Chapter 4: Results & Discussion	50
4.1 Calculation of important parameters (Y, k _d , K _s , k, µ _m)	
4.1.1 Determination of Y & k _d	51
4.1.2 Determination of K _s , k, μ_m	52
4.1.3 Full-scale plant data University of Moratuwa, Sri Lanka. Electronic Theses & Dissertations www.lib.mrt.ac.lk	57
Chapter 5: Conclusions	65

References

Declaration

I hereby declare that this submission is a result of work carried out by me & to the best of my knowledge, it contains no material previously written or published by another person nor material which has been accepted for the award of any degree or acceptable qualification of a university, or other institute of higher learning except where the due reference to the material is made.

UOM Verified Signature

Indika Upuli Hettiarachchi. December, 2003.



Abstract

Raw rubber processing factories generate large amounts of wastewater containing organic pollutants & various process chemicals. Factory effluents exhibit high BOD (Biochemical Oxygen Demand) & COD (Chemical Oxygen Demand) concentrations, ammonia & suspended solids that are amenable to biological treatment methods.

Rubber Research Institute (RRI) of Sri Lanka developed a novel & cost effective biological effluent treatment technique for rubber-processing effluents discharged by crepe rubber & centrifuged latex factories. Treatment system, based on high rate anaerobic digestion coupled with aerobic stabilization also consists of settling & sand filtration. The main feature of this technique is the use of a low cost, septic tank type anaerobic digester filled up with coir fibres for the attachment of useful microorganisms for effective biological conversion. Biological kinetic expressions have been derived for the design & control of effluent treatment plants where aerobic digestion is used commonly as the only treatment method. The kinetic coefficients in these expressions are widely used in design calculations. For a specified waste, a given biological community & a particular set of operating conditions the kinetic coefficients are fixed. Kinetic coefficients used for the design of domestic effluent treatment plants cannot be applied for the design of industrial effluent treatment plants as the waste composition & biological communities involved are different. Also kinetic coefficients for the anaerobically pretreated wastewater could be very different to those of the raw wastewater even for the same type of waste. No kinetic study has been carried out yet for the RRI developed treatment process for making possible improvements & modifications for optimal operation & performance of the aerobic treatment system to reduce capital, operational & maintenance costs under low loading conditions.

The objective of this study is to find out the kinetic coefficients required for the design of activated sludge process from anaerobically pretreated rubber industry

wastewater. The obtained values of kinetic coefficients were used to model an existing treatment system.

A pilot-scale continuously aerated stirred tank was used as a model reactor. Reactor was operated without a recycle stream & fed with a steady flow of anaerobically pretreated wastewater obtained from a full-scale rubber industry effluent treatment plant. Samples were taken for five different runs at five different mean-cell residence times (θ_c). BOD & MLVSS (Mixed Liquor Volatile Suspended Solids) of each sample for each run were measured according to Standard Methods for the Examination of Water & Wastewater.

The following kinetic coefficients were estimated by a graphical method using measured data & the standard kinetic expressions.

- Y = cell yield coefficient
- o k_d = cell decay coefficient
- o K_s = half-velocity constant in of Moratuwa, Sri Lanka
- k = maximum substrate concentration per unit mass of microorganisms
- $\mu_m = \text{maximum specific growth rate}$).

The obtained kinetic coefficients show significant differences to those of domestic wastewater reported in literature. Maximum substrate concentration per unit mass of microorganisms (k) is less than one-half of the corresponding value for domestic wastewater. This implies more than double the concentration of microorganisms is required to be maintained in the aeration tank than that for domestic wastewater. Half-velocity constant (K_s) is more than double the concentration of the corresponding value for domestic wastewater. It implies that the microorganisms have high affinity to anaerobically digested substrate. This could be expected because most anaerobically digested intermediate products & end products are considered good substrates for heterotrophic organisms. The cell yield coefficient (Y) is comparatively higher & the cell decay coefficient (X_s) relatively lower than those for domestic wastewater leading to a higher μ_m

IV

maximum specific growth rate. Therefore a richer microorganism concentration

could be expected in the aeration tank.

Obtained kinetic coefficients were used to model an existing activated sludge treatment system. The minimum mean-cell residence time calculated with the obtained kinetic coefficients lead to a value of 0. 9 (d) with a safety factor of 3.33 & is within the accepted range for plant operation (2-20). Sludge washouts are very unlikely due to the fulfillment of the condition $\theta_c > 1/\mu_m$ indicating a good waste stabilization. Calculations revealed significant difference between the predicted & operated condition of the plant. The obtained kinetic coefficients were used to optimize the plant operation by estimating sludge recirculation rate, aeration rate & sludge production rate. The findings will help improve the

University of Moratuwa, Sri Lanka. Electronic Theses & Dissertations www.lib.mrt.ac.lk

treatment system design & reduce the associated costs.

Acknowledgement

I wish to thank my supervisor Dr. S.L.J. Wijekoon for the guidance & advice given to me throughout in completing this research project.

I am also grateful to

- o Dr. W. M. G. Seneviratne, Head, Chemical Engineering & Processing unit, Rubber Research Institute of Sri Lanka
- o Mr. K. Subramanium, M.Sc. course coordinator, Chemical & Process Engineering Department, University of Moratuwa
- o Dr. Shantha Walpolage, Mrs. Shantha Maduwage & all the other staff members of Chemical & Process Engineering Department, University of Moratuwa who helped in numerous ways in carrying out the project
- The non-academic staff of Chemical & Process Engineering Department,
 University of Moratuwa especially Mr. H. R. Saraneris, Mr. Shantha Peiris &
 Mrs. Dinusha Martino who provided the assistance in the experimental work
- o Mr. Sarath Siriwardene & the staff of Chemical Engineering & Processing unit, Rubber Research Institute of Sri Lanka
- o Mr. Navindra Alponso, Instructor, Chemical & Process Engineering

 Department, University of Moratuwa
- o Mr.Lalith Gunatilake
- Miss Dumila Panditha
- Mr. Prasanga Gunaratne, Mr. Pubudu Perera & Mr. Madura Ekanayake who were always ready to provide their assistance whenever required.

I will be indebted to Asian Development bank for granting financial assistance for the course of study.

t of Tables page numb	
Table 1: Total rubber production	1
Table 2: The average chemical composition of rubber processing effluents	6
Table 3: Characteristics of wastewaters from concentrated latex manufacture	9
Table 4: Average chemical composition of combined wastewaters & wasteloads	10
Table 5: Standards stipulated by the Central Environmental Authority of	
Sri Lanka for the discharge of wastewater from concentrated latex	
production into inland waters	10
Table 6: Wastewater characteristics of crepe rubber manufacturing	15
Table 7: Standards stipulated by the Central Environmental Authority of Sri Lanka for the discharge of natural rubber industry wastewater into inland waters	16
Table 8: Average performance & operating conditions of the ASP	4 9
Table 9: Substrate & biomass concentrations for the five runs	59
Table 10: Comparison of kinetic coefficients for domestic, rubber & soap indus wastewater	try 57
AA 19310 AA 1920 T	51
Table 11:Full-scale plant data	58
Table 12: Predicted operating conditions of the full-scale ASP using kinetic	
Coefficients for domestic wastewater & from this study	64

List of Figures	page number
Figure 1: Concentrated latex production process	8
Figure 2: Processing latex into crepe rubber	12
Figure 3: Processing latex into sole crepe rubber	13
Figure 4: Processing field coagulated latex into scrap rubber	14
Figure 5: Processing of latex into Ribbed Smoked Sheet Rubber	14
Figure 6: Design of a RRI developed treatment plant	17
Figure 7: The aerobic in nature	72
Figure 8: The anaerobic in nature University of Moraluwa, Sri Lanka.	73
Figure 9: Aerobic digestion mechanism	74
Figure 10: Schematic diagram of the treatment plant adopted by the Rul	ober 74
Research Institute of Sri Lanka (RRI)	
Figure 11: Schematic of a complete-mix reactor without recycle	33
Figure 12: Schematic of complete-mix reactor with cellular recycle & w	vasting 37
from the recycle line	/:
Figure 13: Typical mass balances for Return-sludge control	1/
a) aeration tank mass balance b)secondary clarifier mass balance	75
Figure 14, 14': Plot to determine kinetic coefficients Y & k _d / K _s & k	54/55

ANNEXURES	e number
Annex 1: Consultancy services to rubber industry	67
Annex 2: Reports on the rubber factory wastewater treatment & dispos	
Rubber production in Sri Lanka	69
Annex 3: Technologies of wastewater treatment used in the Sri Lankan	l
rubber industry	70
Annex 4: Technologies of wastewater treatment used in the Sri Lankan	L
rubber industry	71·
Annex 5: Figure 7: The aerobic in nature	71
Annex 6: Figure 8: The anaerobic in nature	73
Annex 7: Figure 9: Aerobic digestion mechanism	
Figure 10: Schematic diagram of the treatment plant adopted	by
the Rubber Research Institute of Sri Lanka	74
(RRI)	
Annex 8: Figure 13: Typical suspended solids mass balances for	
Return-sludge control	
a)aeration tank mass balance	
b)secondary clarifier mass balance	75
Annex 9: BOD & COD removal efficiencies & variation of pH after	
anaerobic treatment	76
Annex 10: COD removal efficiencies of aerobic treatment	77

/18
79
79



List of symbols & acronyms

d = day $d^{-1} = day^{-1}$

dX/dt = rate of change of microorganism concentration in the reactor measured in terms of mass(VSS), mass VSS/(volume.time)

E = process efficiency

K_o = half-velocity constant, mass/volume

 $k = \mu_m/Y$, maximum rate of substrate utilization per unit mass of microorganisms, time⁻¹

k_d = endogenous decay coefficient, time⁻¹

 N_0 = influent TKN, mass/volume N = effluent TKN, mass/volume

 P_{π} = net weight of activated sludge produced each day, measured in terms of VSS, lb/d (kg/d)

Q = flow rate, volume/time

Q'w = cell wastage rate from recycle line, volume/time

Q_e= flow rate of effluent from the solids separation unit, volume/time

r_g = rate of bacterial growth, mass/volume.time

r_{su} = substrate utilization rate, mass/volume.time

r's = net rate of bacterial growth, mass/volume.time

 r_T = reaction rate at T

 r_{20} = reaction rate at 20° C

S = concentration of growth limiting substrate in solution or substrate concentration in effluent, mass/volume

 S_0 = substrate concentration in influent, mass/volume

 S_0 -S = mass concentration of substrate utilized, mass/volume

t = tomne

T = temperature.°C

U = specific substrate utilization rate, time⁻¹

 $V_r = volume of the reactor$

 V_s = volume of the settling tank

 V_T = volume of reactor plus volume of settling tank

 X_0 = concentration of microorganisms in the influent, mass VSS/volume

X = concentration of microorganisms in the reactor, mass VSS/volume

 X_r = microorganism concentration in return sludge line, mass VSS/volume X_e = microorganism concentration in effluent from the solids separation unit, mass VSS/volume

Y = maximum yield coefficient, mg/mg (ratio of the mass of cells formed to the mass of substrate consumed, measured during any finite period of logarithmic growth) $Y_{obs} = observed$ yield,

 θ = hydraulic retention time

 θ_c = mean cell-residence time

 θ_{ct} = mean cell- residence time based on the total system

 $1/\theta_c$ = net specific growth rate

'θ' = temperature activity coefficient

 μ = specific growth rate, time⁻¹

μ_m= maximum specific growth rate, time⁻¹

 μ' = net specific growth rate, time⁻¹

ASP = Activated Sludge Process

BOD = Biochemical Oxygen Demand

COD = Chemical Oxygen Demand

DO = Dissolved Oxygen

DRC = Dry Rubber Content

IRRDB = International Rubber Research Development Board

MLSS = Mixed Liquor Suspended Solids

MLVSS = Mixed Liquor Volatile Suspended Solids

OUR = Oxygen Uptake Rate

RAS = Return Activated-Sludge

RCCSR = Rubberized Coir Carrier Septic Tank Reactor

RRI = Rubber Research Institute

RRIM = Rubber Research Institute of Malaysia

RSS = Ribbed Smoked Sheet

SBR = Sequencing Batch Reactor

SOUR = Specific Oxygen Uptake Rate

TKN = Total Kjeldal Nitrogen

TMTD = Tetra-Methyl-Thiuram-Disulphide

TOC = Total Organic Carbon

TSR = Technically Specified Rubber

WAS = Waste Activated-Sludge