## CHAPTER 8

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## Appendix1

## Observations of Specific Gravity Test

Table A1.1:Specific Gravity Test of Clayey Sample

| No | Description | Sample 1 | Sample 2 |
| :---: | :--- | :---: | :---: |
| 1 | Temperature in ${ }^{0} \mathrm{C}$ | 31 | 31 |
| 2 | Weight of bottle $\left(\mathrm{W}_{1}\right)$ in g | 18.57 | 18.50 |
| 3 | Weight of bottle + Dry clayey soil $\left(\mathrm{W}_{2}\right)$ in g | 28.57 | 28.50 |
| 4 | Weight of bottle + clayey soil + water $\left(\mathrm{W}_{3}\right)$ in g | 90.88 | 90.20 |
| 5 | Weight of bottle + Water $\left(\mathrm{W}_{4}\right)$ in g | 84.74 | 84.12 |

## Specimen Calculations of Specific Gravity Test

From Table A1.1, set of readings for sample 1;

Specific gravity $(G)$ of the clayey soil $=\left(\mathrm{W}_{2}-\mathrm{W}_{1}\right) /\left[\left(\mathrm{W}_{4}-\mathrm{W}_{1}\right)-\left(\mathrm{W}_{3}-\mathrm{W}_{2}\right)\right]$

$$
\begin{aligned}
& =(28.57-18.57) /[(84.74-18.57)-(90.88-28.57) \\
& =2.59
\end{aligned}
$$

Similarly;

From Table A1.1, set of readings for sample 2;

Specific gravity (G) of the clayey soil $=\left(\mathrm{W}_{2}-\mathrm{W}_{1}\right) /\left[\left(\mathrm{W}_{4}-\mathrm{W}_{1}\right)-\left(\mathrm{W}_{3}-\mathrm{W}_{2}\right)\right]$

$$
\begin{aligned}
& =(28.50-18.50) /[(84.12-18.50)-(90.20-28.50) \\
& =2.55
\end{aligned}
$$

Average specific gravity $(\mathrm{G})$ of the clayey soil $=(2.59+2.55) / 2$

$$
=2.57
$$

## Appendix2

## Observations of Atterberg Limit Test

Table A2.1:Liquid Limit Test (Penetration method) of Clayey Sample

| Container No. | CP4 | B2 | P6 | 9 |
| :--- | :---: | :---: | :---: | :---: |
| Penetration (mm) | 10.6 | 18.2 | 23.5 | 28.6 |
| Weight of Container (g) | 7.00 | 5.07 | 20.25 | 9.21 |
| Weight of Water +Container(g) | 22.37 | 17.73 | 32.06 | 21.15 |
| Weight of Dry Clayey Soil+ Container (g) | 16.44 | 12.50 | 27.09 | 16.04 |

Table A2.2:Plastic Limit Test of Clayey Sample

| Container No. | 24 F | T |
| :--- | :---: | :---: |
| Weight of Wet Clayey Soil + Container (g ) | 24.73 | 20.65 |
| Weight of Dry Clayey Soil + Container ( g ) | 19.86 | 15.35 |
| Weight of Container (g ) | 10.26 | 5.07 |

## Specimen Calculations of Atterberg Limit Test

From Table A2.1, first set of readings for sample CP4;

```
Weight of Wet Clayey Soil + Container (g) \(=22.37\)
Weight of Dry Clayey Soil + Container (g) = 16.44
Weight of Container (g)
\(=7.00\)
Weight of Water (g)
\[
=5.93
\]
\[
\text { Weight of Dry Clayey Soil (g) }=9.44
\]
Moisture Content (\%) = (5.93 / 9.44) x 100\%
\[
\text { = } 62.8 \text { \% }
\]
```

From Table A2.2, first set of readings for sample 24F;

Weight of Wet Clayey Soil + Container (g) = 24.73
Weight of Dry Clayey Soil + Container (g) = 19.86

Weight of Container (g)
Weight of Water (g)
Weight of Dry Clayey Soil (g)
Moisture Content (\%)
= 50.7\%

Similarly, from Table A2.2, calculation for moisture content of B2, P6, 9 and 18samples can be done and tabulated below;

Table A2.3: Moisture Content Results of Liquid Limit Test

| Container No. | CP4 | B2 | P6 | 9 |
| :--- | :---: | :---: | :---: | :---: |
| Weight of Water (g) | 5.93 | 5.23 | 4.97 | 5.11 |
| Weight of Dry Clayey Soil (g) | 9.44 | 7.43 | 6.84 | 6.83 |
| Moisture Content (\%) | 62.8 | 70.5 | 72.6 | 74.8 |

Penetration method for obtaining liquid limit of sample (Moisture content Vs. Penetration) is shown graphically in Figure A2.1.


Figure A2.1: Graph of Moisture Content vs. Penetration

Then;
Liquid Limit of clayey sample (\%) $=70$

Table A2.4: Moisture Content Results of Plastic Limit Test

| Container No. | 24 F | T |
| :--- | :---: | :---: |
| Weight of Water (g) | 4.87 | 5.3 |
| Weight of Dry Clayey Soil (g) | 9.6 | 10.28 |
| Moisture Content (\%) | 50.7 | 51.6 |

Then;
Water content of first sample (\%) =50.7
Water content of second sample (\%)=51.6
Plastic Limit of Clayey sample (\%) $=(50.7+51.6) / 2$

$$
=51.2
$$

Therefore;
Plasticity Indexof Clayey sample(\%) = 70.0-51.2
$=18.8$

## Appendix3

## Observations of Moisture Content Test

Table A3.1:Moisture Content Test of Clayey Model

| No | Description | Top | Middle | Bottom |
| :---: | :--- | :---: | :---: | :---: |
| 1 | Weight of empty container $\left(\mathrm{W}_{1}\right)$ in g | 5.07 | 7.00 | 20.25 |
| 2 | Weight of container+ wet clayey soil $\left(\mathrm{W}_{2}\right)$ in g | 24.13 | 23.47 | 39.23 |
| 3 | Weight of container+ dry clayey soil $\left(\mathrm{W}_{3}\right)$ in g | 16.98 | 17.27 | 32.13 |

## Specimen Calculations of Moisture Content Test

From Table A3.1, set of readings for top sample of clayey model;
Moisture content (w) of topsample of clayey model $=\left[\mathrm{W}_{2}-\mathrm{W}_{3}\right] /\left[\mathrm{W}_{3}-\mathrm{W}_{1}\right] * 100 \%$

$$
\begin{aligned}
& =[24.13-16.98] /[16.98-5.07] * 100 \% \\
& =60 \%
\end{aligned}
$$

Similarly, from Table A3.1, calculation of moisture content of middle and bottom samples of clayey model can be done and results can be as follows;

- Moisture content (w) of middle sample of clayey model $=60.3 \%$
- Moisture content (w) of bottom sample of clayey model = 59.8\%
- Average moisture content $(\mathrm{w})$ of clayey model $=(60+60.3+59.8) / 3$

$$
=60.03 \%
$$

## Appendix4

## Observations of Hydrometer Analysis Test

Table A4.1: Hydrometer Analysis Test of Clayey Sample

| Weight of Sample (g) $=50$ <br> Meniscus Correction $C_{m}$ $=0.5$ <br> Dispersing Agent Correction $C_{d}$ $=2.0$ |  | $\begin{aligned} & G_{s} \\ & \mathrm{~K} \\ & \mathrm{a} \end{aligned}$ | $\begin{aligned} & =2.57 \\ & =0.01246 \\ & =1.015 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Temperature $\left({ }^{0} \mathrm{C}\right)$ | $\begin{aligned} & \text { Time } \\ & \text { (min) } \end{aligned}$ |  | $R_{H}^{\prime}$ |
| 30 | 0.5 |  | 46.9 |
| 30 | 1 |  | 45.2 |
| 30 | 2 |  | 39.7 |
| 30 | 4 |  | 34.4 |
| 30 | 8 |  | 31.8 |
| 30 | 15 |  | 30.7 |
| 30 | 30 |  | 28.3 |
| 30 | 60 |  | 26.6 |
| 30 | 120 |  | 26.0 |
| 30 | 240 |  | 25.4 |

## Specimen Calculations of Hydrometer Analysis Test

From Table A4.1, \% Finer and Diameter of particle after 0.5 minute can be calculated as follows;
Hydrometer reading $R_{H}^{\prime} \quad=46.9$
After Meniscus correction $\mathrm{R}_{\mathrm{H}} \quad=46.9+0.5\left(\mathrm{C}_{\mathrm{m}}=0.5 \mathrm{~g} / \mathrm{l}\right)$

$$
=47.4
$$

Value of L from table provided with the hydrometer $=8.5$
Diameter of a particle from Stroke's law D $\quad=K \sqrt{\frac{L}{t}}$
( $\mathrm{K}=0.01246$ at $30^{\circ} \mathrm{C}$ temperature and 2.57 specific gravity of clay particles according to table provided with the hydrometer)

$$
\begin{aligned}
& =0.01246 \sqrt{\frac{8.5}{0.5}} \\
& =0.05137 \mathrm{~mm} \rightarrow 0.051 \mathrm{~mm}
\end{aligned}
$$

After dispersing agent correction $R=R_{H}-C_{d}=R_{H}^{\prime}-\left(C_{d}-C_{m}\right)$

$$
\begin{aligned}
& =47.4-2\left(\mathrm{C}_{\mathrm{d}}=2 \mathrm{~g} / \mathrm{l}\right) \\
& =45.4
\end{aligned}
$$

Percentage of soil remaining in suspension $P=\frac{R a}{W} \times 100 \%$
( $a=1.015$ at 2.57 specific gravity of soil particles and taken as 1.0 )

$$
\begin{aligned}
& =\frac{45.4 \times 1.0}{50} \times 100 \% \\
\% \text { Finer } & =90.7 \%
\end{aligned}
$$

Similarly, from Table A4.1, calculation for \% Finer and Diameter of particle can be obtained after 1 min, $2 \mathrm{~min}, 4 \mathrm{~min}, 8 \mathrm{~min}, 15 \mathrm{~min}, 30 \mathrm{~min}, 1 \mathrm{hr}, 2 \mathrm{hrs}$ and 4 hrs respectively and tabulated below;

Table A4.2:Results of Hydrometer Analysis Test

| Time <br> $(\mathrm{min})$ | $R_{H}^{\prime}$ | $R_{H}=$ <br> $R_{H}^{\prime}+C_{m}$ | L <br> $(\mathrm{cm})$ | $\mathrm{L} / \mathrm{t}$ | D <br> $(\mathrm{mm})$ | $R=R_{H}-C_{d}$ | \% Finer $\quad P=\frac{R a}{W} \times 100$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.5 | 46.9 | 47.4 | 8.5 | 17 | 0.051 | 45.4 | 90.7 |
| 1 | 45.2 | 45.7 | 8.8 | 8.8 | 0.044 | 43.7 | 87.4 |
| 2 | 39.7 | 40.2 | 9.7 | 4.85 | 0.032 | 38.2 | 76.4 |
| 4 | 34.4 | 34.9 | 10.6 | 2.65 | 0.022 | 32.9 | 65.8 |
| 8 | 31.8 | 32.3 | 11.1 | 1.3875 | 0.015 | 30.3 | 60.5 |
| 15 | 30.7 | 31.2 | 11.2 | 0.7467 | 0.011 | 29.2 | 58.4 |
| 30 | 29.9 | 29.4 | 11.5 | 0.3833 | 0.008 | 27.4 | 54.8 |
| 60 | 29.3 | 28.8 | 11.9 | 0.1983 | 0.006 | 26.8 | 53.5 |
| 120 | 29.0 | 28.5 | 11.95 | 0.099583 | 0.004 | 26.5 | 52.9 |
| 240 | 29.2 | 28.2 | 12.0 | 0.05 | 0.002 | 26.2 | 52.3 |

Finally, Graph of Percentage of Finer vs. Particle Size (Diameter of particle) can be drawn.


Figure A4.1:Graph of Percentage of Finer vs. Particle Size (Diameter of particle)

From above details of hydrometer analysis test, activity of soil(A) can be calculated as follows;

Activity of soil(A) = Plasticity Index / Percent of clay-sized particles (less than $2 \mu \mathrm{~m}$ )
$=18.8 / 52.3$
$=0.36$

## Appendix 5

## Observations of Standard Proctor Compaction Test

- $\quad$ Mass of the mould $=1.954 \mathrm{~kg}$
- Volume of the mould $=944^{*} 10^{-6} \mathrm{~kg} \mathrm{~m}^{-3}$

Table A5.1: Standard Proctor Compaction Test of Clayey Sample

| No | Mass of the <br> mould + soil <br> $(\mathrm{g})$ | Mass of empty can <br> (g) |  | Mass of wet soil + can |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Bottom sample | Top <br> sample | Bottom <br> sample |  |
| 1 | 3.493 | 9.83 | 9.17 | 141.35 | 165.04 |
| 2 | 3.550 | 9.54 | 9.34 | 142.70 | 167.45 |
| 3 | 3.648 | 10.24 | 9.80 | 150.80 | 158.50 |
| 4 | 3.749 | 10.58 | 10.50 | 134.36 | 140.60 |
| 5 | 3.757 | 9.56 | 10.80 | 144.56 | 145.70 |
| 6 | 3.751 | 11.78 | 9.45 | 157.80 | 160.46 |
| 7 | 3.671 | 10.70 | 11.96 | 147.30 | 150.40 |

## Specimen Calculations of Standard Proctor Compaction Test

For first sample;
Mass of the soil $=($ Mass of the mould + soil $)-($ Mass of the mould $)$
$=3.493 \mathrm{~kg}-1.954 \mathrm{~kg}$
$=1.539 \mathrm{~kg}$

Bulk density $\quad=($ Mass of the soil $) /($ Volume of the mould $)$
$=1.539 / 944 * 10^{-6} \mathrm{~kg} \mathrm{~m}^{-3}$
$=1629.98 \mathrm{~kg} \mathrm{~m}-3$

Moisture content $=(\underline{\text { Mass of the wet soil }+ \text { can }) ~}-($ Mass of the dry soil + can $) * 100$ for top sample (Mass of the dry soil + can - Mass of the can)

$$
=(\underline{141.35-124.93}) * 100 \%
$$

(124.93-9.83)

$$
\text { = } 14.27 \text { \% }
$$

Moisture content $=(165.04-145.47) * 100$
for bottom sample (145.47-9.17)

$$
=14.36 \%
$$

$$
\begin{aligned}
\text { Average moisture content } & =14.27 \frac{+14.36}{2} \\
& =14.315 \%
\end{aligned}
$$

Dry density $=\frac{\text { Bulk density }}{\left(1+\frac{\text { moisture content })}{}\right.}$

$$
=1629.98
$$

$$
1+0.14315
$$

$$
=1425.87 \mathrm{~kg} \mathrm{~m}^{-3}
$$

Similarly, from Table A5.1, calculation for Dry Density and Moisture Content of other samples can be obtained and tabulated below;

Table A5.2:Dry Density and Moisture Contentof Other Samples

| Dry Density $\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ | Moisture Content(\%) |
| :---: | :---: |
| 1425.87 | 14.315 |
| 1455.10 | 16.155 |
| 1513.62 | 18.555 |
| 1576.71 | 20.610 |
| 1556.45 | 22.730 |
| 1543.55 | 23.315 |
| 1437.24 | 26.585 |

Calculation for Dry density at $100 \%$ saturation (theoretical) to plot zero air void line can be done using equation-02;
$\rho_{d, \max }=\frac{G \rho_{w}}{1+w G}$ Equation - 02


Where;
Specific Gravity (G) = 2.57
Density of Water $\left(\mathrm{P}_{\mathrm{w}}\right)=1000 \mathrm{~kg} \mathrm{~m}^{-3}$
w = Moisture Content

For sample 01,
Dry density $=\underline{2.57 \times 1000}$

$$
(1+0.14315 \times 2.57)
$$

$=1878.79 \mathrm{~kg} \mathrm{~m}^{-3}$

Similarly values of dry density at $100 \%$ saturation can be calculated at different moisture content and tabulated below.

Table A5.3:Dry DensityValuesat 100\% Saturation

| Sample No | Moisture Content (\%) | Dry Density $\left(\mathrm{kg} \mathrm{m}^{-3}\right)$ |
| :---: | :---: | :---: |
| 01 | 14.315 | 1878.79 |
| 02 | 16.155 | 1815.99 |
| 03 | 18.555 | 1740.13 |
| 04 | 20.610 | 1680.07 |
| 05 | 22.730 | 1622.27 |
| 06 | 23.315 | 1607.05 |
| 07 | 26.585 | 1526.85 |

## Appendix 6

## Observations of Consolidation Test

Table A6.1:Clayey Sample Details


Table A6.2:Consolidation Test of Clayey Sample

| Time(min) | Settlement Corresponding to the Different Loads |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | First Day <br> 25 kPa | Second Day <br> 50 kPa | Third Day <br> 75 kPa | Fourth Day <br> 100 kPa |
| 0 | 0.000 | 1.160 | 1.666 | 2.020 |
| 0.25 | 0.212 | 1.202 | 1.690 | 2.040 |
| 0.5 | 0.236 | 1.210 | 1.698 | 2.044 |
| 1 | 0.262 | 1.218 | 1.712 | 2.050 |
| 2 | 0.298 | 1.232 | 1.721 | 2.058 |
| 4 | 0.360 | 1.252 | 1.742 | 2.068 |
| 8 | 0.436 | 1.286 | 1.764 | 2.082 |
| 15 | 0.502 | 1.328 | 1.790 | 2.100 |
| 30 | 0.626 | 1.392 | 1.822 | 2.128 |
| 60 | 0.772 | 1.462 | 1.858 | 2.162 |
| 120 | 0.938 | 1.532 | 1.898 | 2.208 |
| 240 | 1.052 | 1.586 | 1.936 | 2.240 |
| 1440 | 1.160 | 1.666 | 2.020 | 2.332 |

## Specimen Calculations of Consolidation Test

Table A6.3:SpecimensCalculation

| WEIGHINGS |  |  | Initial specimen <br> (a) |  | (b) |  | al specimen <br> (c) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wet soil + +ring + tray | g |  | 50.80 |  | 142.22 |  | 67.92 |
| Dry soil + +ming+tray | g |  | 38.92 |  | 122.85 |  | 53.82 |
| Ring + tray | g |  | 19.23 |  | 90.73 |  | 30.53 |
| Wet soil | g | $\mathrm{m}_{0}$ | 31.57 | $\mathrm{m}_{0}$ | 51.49 |  | 37.39 |
| Dry soil | g | $\mathrm{m}_{\mathrm{d}}$ | 19.69 | $\mathrm{m}_{\mathrm{d}}$ | 32.12 | $\mathrm{m}_{\mathrm{d}}$ | 23.3 |
| Water | g |  | 11.88 |  | 19.37 |  | 14.10 |
| Moisture content (measured) | \% |  | 60.3 |  | 60.3 |  | 61.0 |
| Moisture content (fromtrimmings) | \% | $\mathrm{W}_{0}$ |  |  | 60.3 |  |  |
| Density | $\mathrm{Mg} / \mathrm{m}^{3}$ |  |  |  | 1.31 |  | 0.95 |
| Dry density | $\mathrm{Mg} / \mathrm{m}^{3}$ |  |  |  | 0.82 |  | 0.59 |
| Voids ratio |  | $\mathrm{e}_{0}$ |  |  | 2.143 |  | 3.35 |
| Degree of saturation | \% | $\mathrm{S}_{0}$ |  |  | 72.4 |  | 46.9 |
| Height of solids | $\mathrm{H}_{\mathrm{s}} \mathrm{mm}$ |  |  |  | 6.36 |  | 4.07 |

Table A6.4:Consolidation TestCalculation

| VOIDS RATIO |  |  |  |  | COMPRESSIBILITY |  |  | COEFFICIENT OF CONSOLIDATION |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Increment | Pressure | Cumulative | Consolidated | Voids | Incremental |  | $\mathrm{m}_{\mathrm{v}}=$ |  | H $=$ | $\mathrm{C}_{\mathrm{V}}$ | k |
|  |  |  |  |  | height | pressure | ठH. 1000 |  | 1/2( $\mathrm{H}_{1}+\mathrm{H}_{2}$ ) | $0.11{ }^{-1} \mathrm{H}^{2}$ | $=c_{v}{ }^{*} \mathrm{~m}_{\mathrm{v}}{ }^{*} \gamma_{\mathrm{w}}$ |
| No. | P | Compression | height | ratio | change | change | $\mathrm{H}_{1} \quad \delta \mathrm{p}$ | $\mathrm{t}_{90}$ |  | $\mathrm{t}_{90}$ |  |
|  |  | ( $\Delta \mathrm{H}-\mathrm{Y}$ ) | $\mathrm{H}=$ | e= | סH | $\delta \mathrm{p}$ |  |  |  |  | * $10^{-7} \mathrm{~mm} / \mathrm{s}$ |
|  |  |  | Но-( $\Delta \mathrm{H}-\mathrm{Y}$ ) | H- $\mathrm{H}_{\text {S }}$ | $=\mathrm{H}_{1}-\mathrm{H}_{2}$ |  |  |  |  |  | (Clay range) |
| N | kPa |  |  | $\mathrm{H}_{S}$ | mm | kPa | $\mathrm{m}^{2} / \mathrm{MN}$ | min | mm | $\mathrm{m}^{2} /$ Year |  |
| 0 | 0 | 0 | 20.000 | 2.143 |  |  |  |  |  |  |  |
| L1 | 25.000 | 1.160 | 18.840 | 1.960 | 1.160 | 25.00 | 2.320 | 43.560 | 19.420 | 0.961 | 7 |
| L2 | 50.000 | 1.666 | 18.334 | 1.881 | 0.506 | 25.00 | 1.074 | 88.360 | 18.587 | 0.434 | 1 |
| L3 | 75.000 | 2.020 | 17.980 | 1.825 | 0.354 | 25.00 | 0.772 | 100.000 | 18.157 | 0.366 | 1 |
| L4 | 100.000 | 2.332 | 17.668 | 1.776 | 0.312 | 25.00 | 0.694 | 141.610 | 17.824 | 0.249 | 1 |

According to above calculations, Consolidation test graphs of clayey sample can be drawn as follow.

## Consolidation Test Graphs



Figure A6.1: Consolidation Graph for 25 kPa Load


Figure A6.2: Consolidation Graph for 50 kPa Load


Figure A6.3: Consolidation Graph for 75 kPa Load


Figure A6.4: Consolidation Graph for 100 kPa Load

## Appendix 7

## Observations of Organic Content Test

- The mass of an empty, clean, and dry porcelain dish $\left(\mathrm{M}_{\mathrm{P}}\right)(\mathrm{g})=40.32$
- The mass of the dish and soil specimen $\left(\mathrm{M}_{\mathrm{PDS}}\right)(\mathrm{g})=49.73$
- The mass of the dish containing the ash (burned soil) $\left(\mathrm{M}_{\mathrm{PA}}\right)(\mathrm{g})=48.60$


## Specimen Calculations of Organic Content Test

The mass of the dry soil $\left(\mathrm{M}_{\mathrm{D}}\right) \quad=\mathrm{M}_{\mathrm{PDS}}-\mathrm{M}_{\mathrm{P}}$

$$
=49.73-40.32
$$

$=9.41 \mathrm{~g}$
The mass of the ashed (burned) soil $\left(\mathrm{M}_{\mathrm{A}}\right)=\mathrm{M}_{\mathrm{PA}}-\mathrm{M}_{\mathrm{P}}$

$$
=48.60-40.32
$$

$=8.28 \mathrm{~g}$
The mass of organic matter $\left(\mathrm{M}_{\mathrm{O}}\right) \quad=\mathrm{M}_{\mathrm{D}}-\mathrm{M}_{\mathrm{A}}$

$$
=9.41-8.28
$$

$$
=1.13 \mathrm{~g}
$$

The organic matter (content) $(O M)=\left(\mathrm{M}_{\mathrm{O}} / \mathrm{M}_{\mathrm{D}}\right) * 100$
$=1.13 / 9.41$

$$
=12 \%
$$

The organic matter (content) of given clayey sample is $12 \%$.

## Appendix 8

## Observations of AIV, ACV and LAAV Tests

Table A8.1: Aggregate Impact Value Test of Concrete Debris

| Test No. | $\mathbf{1}$ | 2 |
| :--- | ---: | ---: |
| Weight of sample (g) | 248.6 | 248.2 |
| Weight of sample passing 2.36 mm sieve <br> after test (g) | 78.8 | 75.2 |
| Weight of sample retained on 2.36 mm sieve <br> after test (g) | 169.8 | 173.0 |

Table A8.2: Aggregate Impact Value Test of Aggregates

| Test No. | $\mathbf{1}$ | 2 |
| :--- | ---: | ---: |
| Weight of sample (g) | 303.4 | 303.4 |
| Weight of sample passing 2.36 mm sieve <br> after test (g) | 74.7 | 77.0 |
| Weight of sample retained on 2.36 mm sieve <br> after test (g) | 228.4 | 226.5 |

## Specimen Calculation

From Table A8.1, $2^{\text {nd }}$ set of readings,
Weight of sample in standard measure
$=248.2 \mathrm{~g}$
Weight of sample passing 2.36 mm sieve after test

$$
=75.2 \mathrm{~g}
$$

Weight of sample retained on 2.36 mm sieve after test $=158.3 \mathrm{~g}$

Hence, Aggregate Impact Value of concrete debris $=30.3$ \%

Similarly,
From $1^{\text {st }}$ set of readings, Aggregate Impact Value $=31.7 \%$
Hence, Average Aggregate Impact Value of concrete debris $=31 \%$

Note: Plaster debris sample was not be prepared for Aggregate Impact Value Test as it was broken into small particles when preparing sample.

Table A8.3: Aggregate Crushing Value Test of Concrete Debris

| Test No. | 1 | 2 |
| :--- | ---: | ---: |
| Weight of sample in standard measure (g) | 2181 | 2185 |
| Weight of sample passing 2.36 mm sieve <br> after test (g) | 761 | 767 |
| Weight of sample retained on 2.36 mm sieve <br> after test (g) | 1414 | 1410 |

Table A8.4: Aggregate Crushing Value Test of Aggregates

| Test No. | $\mathbf{1}$ | $\mathbf{2}$ |
| :--- | :--- | :--- |
| Weight of sample in standard measure (g) | 2185 | 2189 |
| Weight of sample passing 2.36 mm sieve <br> after test (g) | 546 | 556 |
| Weight of sample retained on 2.36 mm sieve <br> after test (g) | 1634 | 1629 |

## Specimen Calculation

From Table A8.3, $2^{\text {nd }}$ set of readings,
Weight of sample in standard measure
$=2185 \mathrm{~g}$
Weight of sample passing 2.36 mm sieve after test
$=767 \mathrm{~g}$
Weight of sample retained on 2.36 mm sieve after test

$$
=1410 \mathrm{~g}
$$

Hence, Aggregate Crushing Value of concrete debris

$$
=767 / 2185 \times 100
$$

$$
=35.1 \%
$$

Similarly,
From $1^{\text {st }}$ set of readings, Aggregate Crushing Value $\quad=34.9 \%$
Hence, Average Aggregate Crushing Value of concrete debris = $35 \%$

Note: Plaster debris sample was not be prepared for Aggregate Crushing Value Test as it broken to small particles when preparing sample

Table A8.5: Los Angeles Abrasive Value Test of Concrete Debris

| Test No. | $\mathbf{1}$ | $\mathbf{2}$ |
| :--- | ---: | ---: |
| Total Weight of sample (g) | 5000 | 5000 |
| Weight of sample passing 1.7 mm sieve after <br> test (g) | 2130 | 2070 |
| Weight of sample retained on 1.7 mm sieve <br> after test (g) | 2870 | 2930 |

Table A8.6: Los Angeles Abrasive Value Test of Aggregates

| Test No. | $\mathbf{1}$ | $\mathbf{2}$ |
| :--- | :--- | :--- |
| Total Weight of sample (g) | 5000 | 5000 |
| Weight of sample passing 1.7 mm sieve after <br> test $(\mathrm{g})$ | 1596 | 1544 |
| Weight of sample retained on 1.7 mm sieve <br> after test (g) | 3400 | 3449 |

## Specimen Calculation

From Table A8.5, $2^{\text {nd }}$ set of readings,
Total weight of sample (W1 g) $=5000 \mathrm{~g}$
Weight retained on 1.7 mm sieve after rotation $(\mathrm{W} 2 \mathrm{~g}) \quad=2699 \mathrm{~g}$
Weight passing 1.7 mm sieve after rotation $(\mathrm{W} 2 \mathrm{~g}) \quad=2271 \mathrm{~g}$
Hence, Los Angeles Abrasion Value $=41.4 \%$
Similarly,
From $1^{\text {st }}$ set of readings, Los Angeles Abrasion Value $\quad=42.6 \%$
Hence, Average Los Angeles Abrasion Value of concrete debris = $42 \%$

Note: Plaster debris sample was not be prepared for Los Angeles Abrasive Value Test as it broken to small particles when preparing sample.

## Appendix 9

## Observations of Slake Durability Test

Table A9.1: Slake Durability Test of Brick Debris

| Test date | Initial | After one <br> month | After two <br> months |
| :--- | :---: | :---: | :---: |
| Weight of sample, dry weight basis(g) | 500 | 500 | 500 |
| Weight retained after $1^{\text {st }}$ cycle, dry weight basis(g) | 416 | 413 | 412 |
| Weight retained after $2^{\text {nd }}$ cycle, dry weight basis(g) | 357 | 353 | 346 |

Table A9.2: Slake Durability Test of Concrete Debris

| Test date | Initial | After one <br> month | After two <br> months |
| :--- | :---: | :---: | :---: |
| Weight of sample, dry weight basis(g) | 500 | 500 | 500 |
| Weight retained after $1^{\text {st }}$ cycle, dry weight basis(g) | 479 | 481 | 485 |
| Weight retained after $2^{\text {nd }}$ cycle, dry weight basis(g) | 464 | 470 | 477 |

Table A9.3: Slake Durability Test of Plaster Debris

| Test date | Initial | After one <br> month | After two <br> months |
| :--- | :---: | :---: | :---: |
| Weight of sample, dry weight basis(g) | 500 | 500 | 500 |
| Weight retained after $1^{\text {st }}$ cycle, dry weight basis(g) | 460 | 481 | 479 |
| Weight retained after $2^{\text {nd }}$ cycle, dry weight basis(g) | 459 | 465 | 467 |

## Specimen Calculations of Slake Durability Test

From Table A9.1, Initial set of readings;
Weight of sample,dry weight basis (g) $=500 \mathrm{~g}$
Weight retained after ${ }^{\text {st }}$ cycle, dry weight basis (g) $=416 \mathrm{~g}$
Hence, Slake Indexof Brick debris after $1^{\text {st }}$ cycle $=(416 / 500) \times 100 \%$

$$
=83.2 \%
$$

Weight retained after $2^{\text {nd }}$ cycle, dry weight basis (g) $\quad=357 \mathrm{~g}$
Hence, Slake Index of Brick debris after $2^{\text {nd }}$ cycle $=(357 / 500) \times 100 \%$
=71.4 \%

Similarly;
From after one month set of readings,
Slake Index of Brick debrisafter $1^{\text {st }}$ cycle=82.6 \%
Slake Index of Brick debris after ${ }^{\text {nd }}$ cycle $=70.6 \%$
From after two months set of readings,
Slake Index of Brick debrisafter $1^{\text {st }}$ cycle= $82.4 \%$
Slake Index of Brick debris after ${ }^{\text {nd }}$ cycle $=69.2 \%$

Similarly, calculation was done for concrete block debris and cement plaster separately and values are tabulated below;

Table A9.4: Initial Values of Slake Durability Test of Different Type of Debris

| Sample <br> name | Initial weight,dry <br> weight basis <br> $(\mathrm{g})$ | Weight retained <br> after 1 1 <br> weight basis <br> $(\mathrm{g})$ | \% Weight <br> retained after <br> $1^{\text {st }}$ cycle, dry <br> weight basis | Weight retained <br> after 2 <br> weight basis <br> (g) | \% Weight retained <br> after 2nd <br> weighte, dry |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Concrete | 500 | 479 | 95.8 | 464 | 92.8 |
| Plaster | 500 | 460 | 92.0 | 459 | 91.8 |
| Brick | 500 | 416 | 83.2 | 357 | 71.4 |

Table A9.5:Values of Slake Durability Test of Different Type of Debris after One Month

| Sample <br> name | Initial weight,dry <br> weight basis <br> $(\mathrm{g})$ | Weight retained <br> after 1 1t <br> weight basis <br> $(\mathrm{g})$ | \% Weight <br> retained after <br> $1^{\text {st }}$ cycle, dry <br> weight basis | Weight retained <br> after 2nd cycle, <br> dry weight basis <br> $(\mathrm{g})$ | \% Weight retained <br> after 2nd cycle, dry <br> weight basis |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Concrete | 500 | 481 | 96.2 | 470 | 94.0 |
| Plaster | 500 | 481 | 96.2 | 465 | 93.0 |
| Brick | 500 | 413 | 82.6 | 353 | 70.6 |

Table A9.6:Values of Slake Durability Test of Different Type of Debrisafter Two Months

| Sample <br> name | Initial weight,dry <br> weight basis <br> $(\mathrm{g})$ | Weight retained <br> after 1 <br> weight basis <br> (g) | \% Weight <br> retained after <br> $1^{\text {st }}$ cycle, dry <br> weight basis | Weight retained <br> after 2nd cycle, <br> dry weight basis <br> (g) | \% Weight retained <br> after 2nd cycle, dry <br> weight basis |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Concrete | 500 | 485 | 97.0 | 477 | 95.4 |
| Plaster | 500 | 479 | 95.8 | 467 | 93.4 |
| Brick | 500 | 412 | 82.4 | 346 | 69.2 |

These valuescan be shown graphically in Figure A9.1, FigureA9.2 and FigureA9.3.


Figure A9.1:Initial Slake Index Values of Different Type of Debris


Figure A9.2:Slake Index Values of Different Type of Debris after One Month


Figure A9.3:Slake Index Values of Different Type of Debris after Two Months

## Appendix 10

## Observations of Compressive Strength Test

Table A10.1:Compressive Strength Test of Concrete

| Penetration <br> of Plunger <br> $(\mathrm{cm})$ | Dial <br> Reading of <br> proving ring |
| :---: | :---: |
| 0 | 0 |
| 0.125 | 1 |
| 0.25 | 2 |
| 0.375 | 2 |
| 0.5 | 3 |
| 0.625 | 3 |
| 0.75 | 3 |
| 0.875 | 3 |
| 1 | 4 |
| 1.125 | 4 |
| 1.25 | 4 |
| 1.375 | 4 |
| 1.5 | 4 |
| 1.625 | 4 |
| 1.75 | 5 |
| 1.875 | 5 |
| 2 | 5 |
| 2.125 | 5 |
| 2.25 | 5 |
| 2.375 | 5 |
| 2.5 | 5 |
| 2.625 | 5 |


| 2.875 | 6 |
| :---: | :---: |
| 3 | 6 |
| 3.125 | 6 |
| 3.25 | 6 |
| 3.375 | 6 |
| 3.5 | 7 |
| 3.625 | 7 |
| 3.75 | 7 |
| 3.875 | 7 |
| 4 | 7 |
| 4.125 | 7 |
| 4.25 | 8 |
| 4.375 | 8 |
| 4.5 | 8 |
| 4.625 | 8 |
| 4.75 | 8 |
| 4.875 | 9 |
| 5 | 9 |
| 5.125 | 9 |
| 5.25 | 9 |
| 5.375 | 10 |
| 5.5 | 10 |
| 5.625 | 10 |
| 5.75 | 10 |
| 5.875 | 10 |
| 6 | 10 |

Table A10.2:Compressive Strength Test of Aggregate

| Penetration <br> of Plunger <br> (cm) | Dial Reading <br> of proving <br> ring |
| :---: | :---: |
| 0 | 0 |
| 0.125 | 1 |
| 0.25 | 1 |
| 0.375 | 2 |
| 0.5 | 3 |
| 0.625 | 4 |
| 0.75 | 5 |
| 0.875 | 6 |
| 1 | 6 |
| 1.125 | 6 |
| 1.25 | 7 |
| 1.375 | 7 |
| 1.5 | 7 |
| 1.625 | 7 |
| 1.75 | 7 |
| 1.875 | 8 |
| 2 | 8 |
| 2.125 | 8 |
| 2.25 | 8 |
| 2.375 | 8 |
| 2.5 | 8 |
| 2.625 | 9 |
| 2.75 | 9 |


| 2.875 | 9 |
| :---: | :---: |
| 3 | 9 |
| 3.125 | 9 |
| 3.25 | 10 |
| 3.375 | 10 |
| 3.5 | 10 |
| 3.625 | 10 |
| 3.75 | 10 |
| 3.875 | 10 |
| 4 | 11 |
| 4.125 | 11 |
| 4.25 | 11 |
| 4.375 | 11 |
| 4.5 | 11 |
| 4.625 | 12 |
| 4.75 | 12 |
| 4.875 | 12 |
| 5 | 12 |
| 5.125 | 12 |
| 5.25 | 12 |
| 5.375 | 12 |
| 5.5 | 13 |
| 5.625 | 13 |
| 5.75 | 13 |
| 5.875 | 13 |
| 6 | 13 |
|  |  |

Table A10.3:Compressive Strength Test of Brick

| Penetration of Plunger (cm) | Dial Reading of proving ring |
| :---: | :---: |
| 0 | 0 |
| 0.125 | 1 |
| 0.25 | 1 |
| 0.375 | 1 |
| 0.5 | 1 |
| 0.625 | 1 |
| 0.75 | 1 |
| 0.875 | 1 |
| 1 | 1 |
| 1.125 | 1 |
| 1.25 | 1 |
| 1.375 | 1 |
| 1.5 | 1 |
| 1.625 | 1 |
| 1.75 | 2 |
| 1.875 | 2 |
| 2 | 2 |
| 2.125 | 2 |
| 2.25 | 2 |
| 2.375 | 2 |
| 2.5 | 2 |
| 2.625 | 2 |
| 2.75 | 2 |


| 2.875 | 2 |
| :---: | :---: |
| 3 | 2 |
| 3.125 | 2 |
| 3.25 | 3 |
| 3.375 | 3 |
| 3.5 | 3 |
| 3.625 | 3 |
| 3.75 | 3 |
| 3.875 | 3 |
| 4 | 3 |
| 4.125 | 3 |
| 4.25 | 3 |
| 4.375 | 3 |
| 4.5 | 3 |
| 4.625 | 3 |
| 4.75 | 3 |
| 4.875 | 4 |
| 5 | 4 |
| 5.125 | 4 |
| 5.25 | 4 |
| 5.375 | 4 |
| 5.5 | 4 |
| 5.625 | 4 |
| 5.75 | 4 |
| 5.875 | 4 |
| 6 | 4 |

Table A10.4:Compressive Strength Test of Plaster

| Penetration <br> of Plunger <br> (cm) | Dial Reading <br> of proving <br> ring |
| :---: | :---: |
| 0 | 0 |
| 0.125 | 1 |
| 0.25 | 1 |
| 0.375 | 1 |
| 0.5 | 2 |
| 0.625 | 2 |
| 0.75 | 2 |
| 0.875 | 3 |
| 1 | 3 |
| 1.125 | 3 |
| 1.25 | 3 |
| 1.375 | 3 |
| 1.5 | 3 |
| 1.625 | 3 |
| 1.75 | 4 |
| 1.875 | 4 |
| 2 | 4 |
| 2.125 | 4 |
| 2.25 | 4 |
| 2.375 | 4 |
| 2.5 | 4 |
| 2.625 | 4 |
| 2.75 | 5 |
|  |  |
|  |  |


| 2.875 | 5 |
| :---: | :---: |
| 3 | 5 |
| 3.125 | 5 |
| 3.25 | 5 |
| 3.375 | 5 |
| 3.5 | 5 |
| 3.625 | 5 |
| 3.75 | 5 |
| 3.875 | 5 |
| 4 | 5 |
| 4.125 | 5 |
| 4.25 | 5 |
| 4.375 | 5 |
| 4.5 | 5 |
| 4.625 | 6 |
| 4.75 | 6 |
| 4.875 | 6 |
| 5 | 6 |
| 5.125 | 6 |
| 5.25 | 6 |
| 5.375 | 6 |
| 5.5 | 6 |
| 5.625 | 6 |
| 5.75 | 6 |
| 5.875 | 6 |
| 6 | 6 |
|  |  |
|  |  |

Table A10.5:Compressive Strength Test of Clay

| Penetration <br> of Plunger <br> (cm) | Dial Reading <br> of proving <br> ring |
| :---: | :---: |
| 0 | 0 |
| 0.125 | 1 |
| 0.25 | 2 |
| 0.375 | 2 |
| 0.5 | 3 |
| 0.625 | 3 |
| 0.75 | 3 |
| 0.875 | 3 |
| 1 | 4 |
| 1.125 | 4 |
| 1.25 | 4 |
| 1.375 | 4 |
| 1.5 | 4 |
| 1.625 | 4 |
| 1.75 | 5 |
| 1.875 | 5 |
| 2 | 5 |
| 2.125 | 5 |
| 2.25 | 6 |
| 2.375 | 6 |
| 2.5 | 6 |
| 2.625 | 6 |
| 2.75 | 6 |
| 2.875 | 6 |
|  |  |
|  |  |
| 2 |  |


| 3 | 6 |
| :---: | :---: |
| 3.125 | 7 |
| 3.25 | 7 |
| 3.375 | 7 |
| 3.5 | 7 |
| 3.625 | 7 |
| 3.75 | 7 |
| 3.875 | 8 |
| 4 | 8 |
| 4.125 | 8 |
| 4.25 | 8 |
| 4.375 | 8 |
| 4.5 | 8 |
| 4.625 | 8 |
| 4.75 | 8 |
| 4.875 | 9 |
| 5 | 9 |
| 5.125 | 9 |
| 5.25 | 9 |
| 5.375 | 9 |
| 5.5 | 9 |
| 5.625 | 9 |
| 5.75 | 10 |
| 5.875 | 10 |
| 6 | 10 |
|  |  |

## Appendix 11

## Values of Compressive Strength Test

Table A11.1: Compressive Strength Values of Concrete

| Penetration <br> of Plunger <br> $(\mathrm{cm})$ | Dial Reading <br> of proving <br> ring | Actual <br> Load <br> $(\mathrm{kN})$ |
| :---: | :---: | :---: |
| 0 | 0 | 0.03 |
| 0.125 | 1 | 0.05 |
| 0.25 | 2 | 0.07 |
| 0.375 | 2 | 0.07 |
| 0.5 | 3 | 0.09 |
| 0.625 | 3 | 0.09 |
| 0.75 | 3 | 0.09 |
| 0.875 | 3 | 0.09 |
| 1 | 4 | 0.11 |
| 1.125 | 4 | 0.11 |
| 1.25 | 4 | 0.11 |
| 1.375 | 4 | 0.11 |
| 1.5 | 4 | 0.11 |
| 1.625 | 4 | 0.11 |
| 1.75 | 5 | 0.13 |
| 1.875 | 5 | 0.13 |
| 2 | 5 | 0.13 |
| 2.125 | 5 | 0.13 |
| 2.25 | 5 | 0.13 |
| 2.375 | 5 | 0.13 |
| 2.5 | 5 | 0.13 |
| 2.625 | 5 | 0.13 |
|  |  |  |


| 2.875 | 6 | 0.15 |
| :---: | :---: | :---: |
| 3 | 6 | 0.15 |
| 3.125 | 6 | 0.15 |
| 3.25 | 6 | 0.15 |
| 3.375 | 6 | 0.15 |
| 3.5 | 7 | 0.17 |
| 3.625 | 7 | 0.17 |
| 3.75 | 7 | 0.17 |
| 3.875 | 7 | 0.17 |
| 4 | 7 | 0.17 |
| 4.125 | 7 | 0.17 |
| 4.25 | 8 | 0.19 |
| 4.375 | 8 | 0.19 |
| 4.5 | 8 | 0.19 |
| 4.625 | 8 | 0.19 |
| 4.75 | 8 | 0.19 |
| 4.875 | 9 | 0.21 |
| 5 | 9 | 0.21 |
| 5.125 | 9 | 0.21 |
| 5.25 | 9 | 0.21 |
| 5.375 | 10 | 0.23 |
| 5.5 | 10 | 0.23 |
| 5.625 | 10 | 0.23 |
| 5.75 | 10 | 0.23 |
| 5.875 | 10 | 0.23 |
| 6 | 10 | 0.23 |

Table A11.2: Compressive Strength Values of Aggregate

| Penetration <br> of Plunger <br> (cm) | Dial Reading <br> of proving <br> ring | Actual <br> Load <br> KN |
| :---: | :---: | :---: |
| 0 | 0 | 0.03 |
| 0.125 | 1 | 0.05 |
| 0.25 | 1 | 0.05 |
| 0.375 | 2 | 0.07 |
| 0.5 | 3 | 0.09 |
| 0.625 | 4 | 0.11 |
| 0.75 | 5 | 0.13 |
| 0.875 | 6 | 0.15 |
| 1 | 6 | 0.15 |
| 1.125 | 6 | 0.15 |
| 1.25 | 7 | 0.17 |
| 1.375 | 7 | 0.17 |
| 1.5 | 7 | 0.17 |
| 1.625 | 7 | 0.17 |
| 1.75 | 7 | 0.17 |
| 1.875 | 8 | 0.19 |
| 2 | 8 | 0.19 |
| 2.125 | 8 | 0.19 |
| 2.25 | 8 | 0.19 |
| 2.375 | 8 | 0.19 |
| 2.5 | 8 | 0.19 |
| 2.625 | 9 | 0.21 |
| 2.75 | 9 | 0.21 |


| 2.875 | 9 | 0.21 |
| :---: | :---: | :---: |
| 3 | 9 | 0.21 |
| 3.125 | 9 | 0.21 |
| 3.25 | 10 | 0.23 |
| 3.375 | 10 | 0.23 |
| 3.5 | 10 | 0.23 |
| 3.625 | 10 | 0.23 |
| 3.75 | 10 | 0.23 |
| 3.875 | 10 | 0.23 |
| 4 | 11 | 0.25 |
| 4.125 | 11 | 0.25 |
| 4.25 | 11 | 0.25 |
| 4.375 | 11 | 0.25 |
| 4.5 | 11 | 0.25 |
| 4.625 | 12 | 0.27 |
| 4.75 | 12 | 0.27 |
| 4.875 | 12 | 0.27 |
| 5 | 12 | 0.27 |
| 5.125 | 12 | 0.27 |
| 5.25 | 12 | 0.27 |
| 5.375 | 12 | 0.27 |
| 5.5 | 13 | 0.29 |
| 5.625 | 13 | 0.29 |
| 5.75 | 13 | 0.29 |
| 5.875 | 13 | 0.29 |
| 6 | 13 | 0.29 |

Table A11.3: Compressive Strength Values of Brick

| Penetration <br> of Plunger <br> $(\mathrm{cm})$ | Dial Reading <br> of proving <br> ring | Actual <br> Load <br> KN |
| :---: | :---: | :---: |
| 0 | 0 | 0.03 |
| 0.125 | 1 | 0.05 |
| 0.25 | 1 | 0.05 |
| 0.375 | 1 | 0.05 |
| 0.5 | 1 | 0.05 |
| 0.625 | 1 | 0.05 |
| 0.75 | 1 | 0.05 |
| 0.875 | 1 | 0.05 |
| 1 | 1 | 0.05 |
| 1.125 | 1 | 0.05 |
| 1.25 | 1 | 0.05 |
| 1.375 | 1 | 0.05 |
| 1.5 | 1 | 0.05 |
| 1.625 | 1 | 0.05 |
| 1.75 | 2 | 0.07 |
| 1.875 | 2 | 0.07 |
| 2 | 2 | 0.07 |
| 2.125 | 2 | 0.07 |
| 2.25 | 2 | 0.07 |
| 2.375 | 2 | 0.07 |
| 2.5 | 2 | 0.07 |
| 2.625 | 2 | 0.07 |
| 2.75 | 2 | 0.07 |
|  |  |  |


| 2.875 | 2 | 0.07 |
| :---: | :---: | :---: |
| 3 | 2 | 0.07 |
| 3.125 | 2 | 0.07 |
| 3.25 | 3 | 0.09 |
| 3.375 | 3 | 0.09 |
| 3.5 | 3 | 0.09 |
| 3.625 | 3 | 0.09 |
| 3.75 | 3 | 0.09 |
| 3.875 | 3 | 0.09 |
| 4 | 3 | 0.09 |
| 4.125 | 3 | 0.09 |
| 4.25 | 3 | 0.09 |
| 4.375 | 3 | 0.09 |
| 4.5 | 3 | 0.09 |
| 4.625 | 3 | 0.09 |
| 4.75 | 3 | 0.09 |
| 4.875 | 4 | 0.11 |
| 5 | 4 | 0.11 |
| 5.125 | 4 | 0.11 |
| 5.25 | 4 | 0.11 |
| 5.375 | 4 | 0.11 |
| 5.5 | 4 | 0.11 |
| 5.625 | 4 | 0.11 |
| 5.75 | 4 | 0.11 |
| 5.875 | 4 | 0.11 |
| 6 | 4 | 0.11 |

Table A11.4:Compressive Strength Values of Plaster

| Penetration <br> of Plunger <br> (cm) | Dial Reading <br> of proving <br> ring | Actual <br> Load <br> KN |
| :---: | :---: | :---: |
| 0 | 0 | 0.03 |
| 0.125 | 1 | 0.05 |
| 0.25 | 1 | 0.05 |
| 0.375 | 1 | 0.05 |
| 0.5 | 2 | 0.07 |
| 0.625 | 2 | 0.07 |
| 0.75 | 2 | 0.07 |
| 0.875 | 3 | 0.09 |
| 1 | 3 | 0.09 |
| 1.125 | 3 | 0.09 |
| 1.25 | 3 | 0.09 |
| 1.375 | 3 | 0.09 |
| 1.5 | 3 | 0.09 |
| 1.625 | 3 | 0.09 |
| 1.75 | 4 | 0.11 |
| 1.875 | 4 | 0.11 |
| 2 | 4 | 0.11 |
| 2.125 | 4 | 0.11 |
| 2.25 | 4 | 0.11 |
| 2.375 | 4 | 0.11 |
| 2.5 | 4 | 0.11 |
| 2.625 | 4 | 0.11 |
| 2.75 | 5 | 0.13 |
|  |  |  |


| 2.875 | 5 | 0.13 |
| :---: | :---: | :---: |
| 3 | 5 | 0.13 |
| 3.125 | 5 | 0.13 |
| 3.25 | 5 | 0.13 |
| 3.375 | 5 | 0.13 |
| 3.5 | 5 | 0.13 |
| 3.625 | 5 | 0.13 |
| 3.75 | 5 | 0.13 |
| 3.875 | 5 | 0.13 |
| 4 | 5 | 0.13 |
| 4.125 | 5 | 0.13 |
| 4.25 | 5 | 0.13 |
| 4.375 | 5 | 0.13 |
| 4.5 | 5 | 0.13 |
| 4.625 | 6 | 0.15 |
| 4.75 | 6 | 0.15 |
| 4.875 | 6 | 0.15 |
| 5 | 6 | 0.15 |
| 5.125 | 6 | 0.15 |
| 5.25 | 6 | 0.15 |
| 5.375 | 6 | 0.15 |
| 5.5 | 6 | 0.15 |
| 5.625 | 6 | 0.15 |
| 5.75 | 6 | 0.15 |
| 5.875 | 6 | 0.15 |
| 6 | 6 | 0.15 |

Table A11.5:Compressive Strength Values of Clay

| Penetration <br> of Plunger <br> (cm) | Dial Reading <br> of proving <br> ring | Actual <br> Load <br> KN |
| :---: | :---: | :---: |
| 0 | 0 | 0.03 |
| 0.125 | 1 | 0.05 |
| 0.25 | 2 | 0.07 |
| 0.375 | 2 | 0.07 |
| 0.5 | 3 | 0.09 |
| 0.625 | 3 | 0.09 |
| 0.75 | 3 | 0.09 |
| 0.875 | 3 | 0.09 |
| 1 | 4 | 0.11 |
| 1.125 | 4 | 0.11 |
| 1.25 | 4 | 0.11 |
| 1.375 | 4 | 0.11 |
| 1.5 | 4 | 0.11 |
| 1.625 | 4 | 0.11 |
| 1.75 | 5 | 0.13 |
| 1.875 | 5 | 0.13 |
| 2 | 5 | 0.13 |
| 2.125 | 5 | 0.13 |
| 2.25 | 6 | 0.15 |
| 2.375 | 6 | 0.15 |
| 2.5 | 6 | 0.15 |
| 2.625 | 6 | 0.15 |
| 2.75 | 6 | 0.15 |
| 2.875 | 6 | 0.15 |
|  |  |  |


| 3 | 6 | 0.15 |
| :---: | :---: | :---: |
| 3.125 | 7 | 0.17 |
| 3.25 | 7 | 0.17 |
| 3.375 | 7 | 0.17 |
| 3.5 | 7 | 0.17 |
| 3.625 | 7 | 0.17 |
| 3.75 | 7 | 0.17 |
| 3.875 | 8 | 0.19 |
| 4 | 8 | 0.19 |
| 4.125 | 8 | 0.19 |
| 4.25 | 8 | 0.19 |
| 4.375 | 8 | 0.19 |
| 4.5 | 8 | 0.19 |
| 4.625 | 8 | 0.19 |
| 4.75 | 8 | 0.19 |
| 4.875 | 9 | 0.21 |
| 5 | 9 | 0.21 |
| 5.125 | 9 | 0.21 |
| 5.25 | 9 | 0.21 |
| 5.375 | 9 | 0.21 |
| 5.5 | 9 | 0.21 |
| 5.625 | 9 | 0.21 |
| 5.75 | 10 | 0.23 |
| 5.875 | 10 | 0.23 |
| 6 | 10 | 0.23 |

## Appendix 12

## Observations of Vane Shear Test

Table A12.1: Vane Shear Test at 80 mm Distancefrom Center of Model Initially

| Test Location | Test Depth (mm) | Shear Strength(divisions) fromApparatus for Clay Surrounding |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Aggregate | Concrete | Plaster | Brick | Clay |
| 80 mm from center of model | 0 | 20 | 20 | 21 | 19 | 7.5 |
| 80 mm from center of model | 80 | 26 | 24 | 23 | 22 | 11 |

Table A12.2:Vane Shear Test at 35 mm Distancefrom Center of Model Initially

|  | Test <br> Depth <br> Test Location |  |  | Shear Strength(divisions) fromApparatus for Clay <br> Surrounding |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | Aggregate | Concrete | Plaster | Brick | Clay |  |
| 35 mm from <br> center of model | 0 | 24 | 24 | 24 | 23.5 | 12 |
| 35 mm from <br> center of model | 80 | 32 | 30 | 31 | 29 | 16 |

Table A12.3:Vane Shear Test at 80 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

| Test Location | Test Depth (mm) | Shear Strength(divisions) fromApparatus for Clay Surrounding |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Aggregate | Concrete | Plaster | Brick | Clay |
| 80 mm from center of model | 0 | 26 | 21 | 22 | 20 | 10 |
| 80 mm from center of model | 80 | 36 | 32 | 34 | 34 | 13 |

Table A12.4:Vane Shear Test at 35 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

| Test Location | Test Depth (mm) | Shear Strength(divisions) fromApparatus for Clay Surrounding |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Aggregate | Concrete | Plaster | Brick | Clay |
| 35 mm from center of model | 0 | 34 | 31 | 30 | 32 | 14 |
| 35 mm from center of model | 80 | 40 | 39 | 37 | 38 | 22 |

Table A12.5:Vane Shear Test at 80 mm Distancefrom Center of Model with Load after One Month Soaked Period

| Test Location | Test Depth (mm) | Shear Strength(divisions) fromApparatus for Clay Surrounding |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Aggregate | Concrete | Plaster | Brick | Clay |
| 80 mm from center of model | 0 | 31 | 30 | 29 | 29 | 13 |
| 80 mm from center of model | 80 | 42 | 37 | 36 | 36 | 17 |

Table A12.6:Vane Shear Test at 35 mm Distancefrom Center of Model with Load after One Month Soaked Period

|  | Test <br> Depth <br> Test Location |  |  | Shear Strength(divisions) fromApparatus for Clay <br> (mm) |  |  |  |  | Agrounding |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: |
| 35 mm from <br> center of model | 0 | 37 | 36 | 34 | 36 | 17 |  |  |  |
| 35 mm from <br> center of model | 80 | 45 | 43 | 39 | 42 | 24 |  |  |  |

## Appendix 13

## Shear Strength Values of Clay Surrounding

Table A13.1:Shear Strength Valuesat 80 mm Distancefrom Center of Model Initially

|  | Test | Shear Strength(kPa) of Clay Surrounding |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test Location | Depth <br> $(\mathrm{mm})$ | Aggregate | Concrete | Plaster | Brick | Clay |
| 80 mm from <br> center of model | 0 | 6 | 6 | 6 | 5 | 2 |
| 80 mm from <br> center of model | 80 | 7 | 7 | 6 | 6 | 3 |

Table A13.2:Shear Strength Valuesat 35 mm Distancefrom Center of Model Initially

|  | Test | Shear Strength(kPa) of Clay Surrounding |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test Location | Depth <br> $(\mathrm{mm})$ | Aggregate | Concrete | Plaster | Brick | Clay |
| 35 mm from <br> center of model | 0 | 7 | 7 | 7 | 6.5 | 3 |
| 35 mm from <br> center of model | 80 | 9 | 8 | 9 | 8 | 4 |

Table A13.3:Shear Strength Valuesat 80 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

| Test Location | Test <br> Depth <br> (mm) | Shear Strength(kPa) of Clay Surrounding with load(8 kg ) after 07 days |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Aggregate | Concrete | Plaster | Brick | Clay |
| 20 mm from edge of model | 0 | 7 | 6 | 6 | 6 | 3 |
| 20 mm from edge of model | 80 | 10 | 9 | 9 | 9 | 4 |

Table A13.4:Shear Strength Valuesat 35 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

| Test Location | Test Depth (mm) | Shear Strength(kPa) of Clay Surrounding with load(8 kg ) after 07 days |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Aggregate | Concrete | Plaster | Brick | Clay |
| 35 mm from center of model | 0 | 9 | 9 | 8 | 9 | 4 |
| 35 mm from center of model | 80 | 11 | 11 | 10 | 11 | 6 |

Table A13.5:Shear Strength Valuesat 80 mm Distancefrom Center of Model with Load after One Month Soaked Period

| Test Location | Test Depth (mm) | Shear Strength(kPa) of Clay Surrounding with load(8 kg ) after One Month |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Aggregate | Concrete | Plaster | Brick | Clay |
| 20 mm from edge of model | 0 | 9 | 8 | 8 | 8 | 4 |
| 20 mm from edge of model | 80 | 12 | 10 | 10 | 10 | 5 |

Table A13.6:Shear Strength Valuesat 35 mm Distancefrom Center of Model with Load after One Month Soaked Period

|  | Test | Shear Strength(kPa) of Clay Surrounding with load(8 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test Location | (m) after One Month <br> $(\mathrm{mm})$ |  |  |  | Aggregate | Concrete |
| Telaster | Brick | Clay |  |  |  |  |
| 35 mm from <br> center of model | 0 | 10 | 10 | 9 | 10 | 5 |
| 35 mm from <br> center of model | 80 | 13 | 12 | 11 | 12 | 7 |

## Appendix 14

Table A14.1: Shear Strength Calibration Chart for the 33 mm Blade

| Divisions | kPa | Divisions | kPa | Divisions | kPa | Divisions | kPa |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | 36 | 10 | 71 | 20 | 106 | 30 |
| 2 | 1 | 37 | 10 | 72 | 20 | 107 | 30 |
| 3 | 1 | 38 | 11 | 73 | 20 | 108 | 30 |
| 4 | 1 | 39 | 11 | 74 | 21 | 109 | 30 |
| 5 | 1 | 40 | 11 | 75 | 21 | 110 | 31 |
| 6 | 2 | 41 | 11 | 76 | 21 | 111 | 31 |
| 7 | 2 | 42 | 12 | 77 | 21 | 112 | 31 |
| 8 | 2 | 43 | 12 | 78 | 22 | 113 | 31 |
| 9 | 3 | 44. | 12 | 79 | 22 | 114 | 32 |
| 10 | 3 | 45 | 13 | 80 | 22 | 115 | 32 |
| - 11 | 3 | 46 | 13 | 81 | 23 | 116 | 32 |
| 12 | 3 | 47 | 13 | 82 | 23 | 117 | 33 |
| 13 | 4 | 48 | 13 | 83 | 23 | 118 | 33 |
| 14 | 4 | 49 | 14 | 84 | 23 | 119 | 33 |
| 15 | 4 | 50. | 14 | 85 | 24 | 120 | 33 |
| 16 | 4 | 51 | 14 | 86 | 24 | 121 | 34 |
| 17 | 5 | 52 | 14 | 87 | 24 | 122 | 34 |
| 18 | 5 | 53 | 15 | 88 | 25 | 123 | 34 |
| 19 | 5 | 54 | 15 | 89 | 25 | 124 | 35 |
| 20 | 6 | 55 | 15 | 90 | 25 | 125 | 35 |
| 21 | 6 | 56 | 16 | 91 | 25 | 126 | 35 |
| 22 | 6 | 57 | 16 | 92 | 26 | 127 | 35 |
| 23 | 6 | 58 | 16 | 93 | 26 | 128 | 36 |
| 24 | 7 | 59 | 16 | 94 | 26 | 129 | 36 |
| 25 | 7 | 60 | 17 | 95 | 26 | 130 | 36 |
| 26 | 7 | 61 | 17 | 86 | 27 | 131 | 36 |
| 27 | 8 | 62 | 17 | 97 | 27 | 132 | 37 |
| 28 | 8 | 63 | 18 | 98 | 27 | 133 | 37 |
| 29 | 8 | 64 | 18 | 99 | 28 | 134 | 37 |
| 30 | 8 | 65 | 18 | 100 | 28 | 135 | 38 |
| 31 | 9 | 66 | 18 | 101 | 28 | 136 | 38 |
| 32 | 9 | 67 | 19 | 102 | 28 | 137 | 38 |
| 33 | 9 | 68 | 19 | 103 | 29 | 138 | 38 |
|  | 9 | 69 | 19 | 104 | 29 | 139 | 39 |
| 35 | 10 | 70 | 20 | 105 | 29 | 140 | 39 |

Appendix 15


Figure A15.1: Construction Debris


Figure A15.2: Concrete Debris


Figure A15.3: Brick Debris


Figure A15.4: Cement Plaster Debris

