CHAPTER 8

REFERENCES

- 1 Ambily AP and Gandhi SR (2007) Behavior of stone columns based on experimental and FEM analysis. Journal of Geotechnical and Geo-environmental Engineering, ASCE 133(4): pp. 405-415.
- ASTM (American Society for Testing and Materials) (2004): A.S.T.M D 4644-87, D2573 / D2573M –15 and D 2166 / D2166M 16, D 854, D 4318, D 2216, D 421&422, D 698-00a and D 2974 Standard Methods. Published by ASTM International, West Conshohocken, PA,USA.
- 3 Bryan A. McCabe, James A. McNeill and Jonathan A. Black (2007) Ground Improvement using the Vibro-Stone Column Technique. Presented at the joint meeting of Engineers Ireland West Region and the Geotechnical Society of Ireland, NUI Galway.
- 4 BS (British Standards) (B.S 1377: Part 2, 1990) British Standard Methods of Test for soils for Civil Engineering Purposes. Published by the British Standards Institution, pp. 8-200.
- 5 Chu jian (August 2012) Methods for Land Reclamation Using soft Soil and Waste. NTU-JTC 13C Seminar, Nanyang Technological University, School of Civil and Environmental Engineering.
- 6 Director(R&D). (2006, 2 16). Testing of Road Construction Materials. Colombo, Western, Sri Lanka: Road Development Authority.
- 7 Hughes, J.M.O. and Withers, N.J. (1974) Reinforcing of Soft Cohesive Soils with Stone Columns. Ground Engineering, Vol. 7, No. 3, pp. 42-49.
 - 8 Imtiaz Ahmed (1991) Use of Waste Materials in Highway Construction. Final Report, Department of civil Engineering, Purdue University, West Lafayette, Indiana 47907.
 - Isaac D.S. and Girish M.S. (2009), Suitability of Different Materials for Stone Column Construction.
 Department of Civil Engineering College of Engineering, Trivandrum, Kerala, EJGE, 14 (2009) Bund.
 M.
- 10 Joe Persichetti (2010) Recycled Concrete as Vibro Stone Columns Backfill. Sustainability seminar Hollywood.
 - 11 Kosho A, A.L.T.E.A &Geostudio (2000) Ground Improvement using the Vibro-Stone Column Technique, Durres, Albania.
 - 12 McKelvey, D., Sivakumar, V., Bell, A., and Graham, J. (2004) Modeling Vibrated Stone Columns on Soft Clay. Geo-tech. Eng., 15(GE3), pp.137–149.

- 13 Mitchell, J.K. and Huber, T.R., (1985) Performance of a Stone Column Foundation. Journal of Geochnical Engineering, ASCE 111(2): pp. 193-201.
- 14 Ramanathan A and Sasikala S. (2014) Model Tests on the Use of Tyre Chips as Aggregate in Stone Columns. The Institution of Civil Engineers, Ground Improvement 168, pp. 187-193.
- 15 Soil Improvement and Ground Modification Methods (2015), Emerging Technologies, Trends, and Materials. Chapter 18: pp. 433-434.
- 16 SivakumarV and Glynn D (2004) Geotechnical Aspects of Recycled Construction Wastes. Queen's University of Belfast, United Kingdom. pp. 151-156.
- 17 Sivakumar V, Mckinley J.D and Ferguson D (2002) Reuse of construction waste: Performance under Repeated Loading. Geotechnical Engineering, Vo.157, No. 2, pp. 91-96.
- 18 Siddhartha Kr. Karmakar, Parbin Sultana and AshimKantiDey (December 2016) Use of Jhama Columns as Replacement of Stone Columns.Indian Geotechnical Conference IGC2016, IIT Madras, Chennai, India.

19 Skempton AW, 1953. The Colloidal Activity of Clays. 3rd International Conference Soil Mech found Eng. Switzerland, vol. 1.

20Suriya Pa, Praveen S,PonkarthiJ and NemalipuriKirankumar (2016) Performance of Clay Soil with Different Materials in Stone Column.Department of Civil Engineering, AarupadaiVeeduInstitute of Technology, Chennai – 603104 (T.N.) India.Int. J. Chem. Sci.: 14(S1), 2016, pp. 348-352.

21Standard Specification for Construction and Maintenance of Roads and Bridges, ICTAD SCA 5 (June 2009).

Observations of Specific Gravity Test

Table A1.1:Specific Gravity Test of Clayey Sample

No	Description	Sample 1	Sample 2
1	Temperature in ⁰ C	31	31
2	Weight of bottle (W ₁) in g	18.57	18.50
3	Weight of bottle + Dry clayey soil (W_2) in g	28.57	28.50
4	Weight of bottle + clayey soil + water (W ₃) in g	90.88	90.20
5	Weight of bottle + Water (W_4) in g	84.74	84.12

Specimen Calculations of Specific Gravity Test

From Table A1.1, set of readings for sample 1;

Specific gravity (G) of the clayey soil = $(W_2 - W_1) / [(W_4 - W_1) - (W_3 - W_2)]$

= (28.57 - 18.57) / [(84.74 - 18.57) - (90.88 - 28.57) = 2.59

Similarly;

From Table A1.1, set of readings for sample 2;

Specific gravity (G) of the clayey soil = $(W_2 - W_1) / [(W_4 - W_1) - (W_3 - W_2)]$

= (28.50 - 18.50) / [(84.12 - 18.50) - (90.20 - 28.50)

= 2.55

Average specific gravity (G) of the clayey soil = (2.59 + 2.55)/2

= 2.57

Observations of Atterberg Limit Test

Table A2.1:Liquid Limit Test (Penetration method) of Clayey Sample

Container No.	CP4	B2	P6	9
Penetration (mm)	10.6	18.2	23.5	28.6
Weight of Container (g)	7.00	5.07	20.25	9.21
Weight of Water +Container(g)	22.37	17.73	32.06	21.15
Weight of Dry Clayey Soil+ Container (g)	16.44	12.50	27.09	16.04

Table A2.2:Plastic Limit Test of Clayey Sample

Container No.	24F	Т
Weight of Wet Clayey Soil + Container (g)	24.73	20.65
Weight of Dry Clayey Soil + Container (g)	19.86	15.35
Weight of Container (g)	10.26	5.07

Specimen Calculations of Atterberg Limit Test

From Table A2.1, first set of readings for sample CP4;

Weight of Wet Clayey Soil + Container $(g) = 22.37$					
Weight of Dry Clayey Soil + Container $(g) = 16.44$					
Weight of Container (g)	= 7.00				
Weight of Water (g)	= 5.93				
Weight of Dry Clayey Soil (g)	= 9.44				
Moisture Content (%) $= (5.93 / 9.44) \times 100$					
	= 62.8 %				

From Table A2.2, first set of readings for sample 24F;

Weight of Wet Clayey Soil + Container (g) = 24.73 Weight of Dry Clayey Soil + Container (g) = 19.86

Weight of Container (g)	= 10.26
Weight of Water (g)	= 4.87
Weight of Dry Clayey Soil (g)	= 9.6
Moisture Content (%)	= (4.87/9.6) x 100%
= 50.7%	

Similarly, from Table A2.2, calculation for moisture content of B2, P6, 9 and 18samples can be done and tabulated below;

Table A2.3: Moisture Content Results of Liquid Limit Test

Container No.	CP4	B2	P6	9
Weight of Water (g)	5.93	5.23	4.97	5.11
Weight of Dry Clayey Soil (g)	9.44	7.43	6.84	6.83
Moisture Content (%)	62.8	70.5	72.6	74.8

Penetration method for obtaining liquid limit of sample (Moisture content Vs. Penetration) is shown graphically in Figure A2.1.

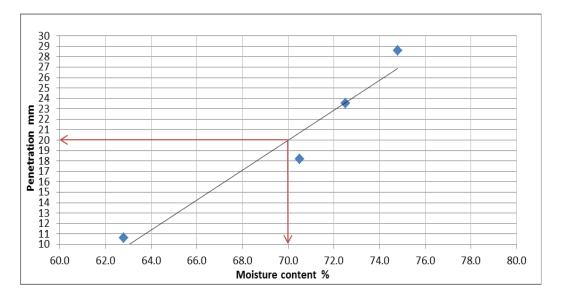


Figure A2.1: Graph of Moisture Content vs. Penetration

Then;

Liquid Limit of clayey sample (%) = 70

Table A2.4: Moisture Content Results of Plastic Limit Test

Container No.	24F	Т
Weight of Water (g)	4.87	5.3
Weight of Dry Clayey Soil (g)	9.6	10.28
Moisture Content (%)	50.7	51.6

Then;

Water content of first sample (%) = 50.7

Water content of second sample (%) = 51.6

Plastic Limit of Clayey sample (%) = (50.7+51.6)/2

= 51.2

Therefore;

Plasticity Indexof Clayey sample(%) = 70.0 - 51.2

= 18.8

Observations of Moisture Content Test

No	Description	Тор	Middle	Bottom
1	Weight of empty container (W ₁) in g	5.07	7.00	20.25
2	Weight of container+ wet clayey soil (W ₂) in g	24.13	23.47	39.23
3	Weight of container+ dry clayey soil (W ₃) in g	16.98	17.27	32.13

Specimen Calculations of Moisture Content Test

From Table A3.1, set of readings for top sample of clayey model;

Moisture content (w) of topsample of clayey model = $[W_2-W_3] / [W_3-W_1]*100\%$

= [24.13 - 16.98] / [16.98 - 5.07]*100%

= 60%

Similarly, from Table A3.1, calculation of moisture content of middle and bottom samples of clayey model can be done and results can be as follows;

- Moisture content (w) of middle sample of clayey model = 60.3%
- Moisture content (w) of bottom sample of clayey model = 59.8%
 - Average moisture content (w) of clayey model = (60 + 60.3 + 59.8)/3

= 60.03%

Observations of Hydrometer Analysis Test

Weight of Sample (Meniscus Correctio Dispersing Agent C	$ \begin{array}{rcl} G_s & = 2.57 \\ K & = 0.01246 \\ a & = 1.015 \end{array} $	
Temperature (⁰ C)	Time (min)	R _H
30	0.5	46.9
30	1	45.2
30	2	39.7
30	4	34.4
30	8	31.8
30	15	30.7
30	30	28.3
30	60	26.6
30	120	26.0
30	240	25.4

Table A4.1: Hydrometer Analysis Test of Clayey Sample

Specimen Calculations of Hydrometer Analysis Test

From Table A4.1, % Finer and Diameter of particle after 0.5 minute can be calculated as follows;

Hydrometer reading R'_H = 46.9 After Meniscus correction R_H = 46.9 + 0.5 (C_m = 0.5 g/l) = 47.4

Value of L from table provided with the hydrometer = 8.5

Diameter of a particle from Stroke's law D = $K \sqrt{\frac{L}{t}}$

(K = 0.01246 at 30° C temperature and 2.57 specific gravity of clay particles according to table provided with the hydrometer)

$$= 0.01246 \sqrt{\frac{8.5}{0.5}}$$

= 0.05137 mm → 0.051 mm

After dispersing agent correction $R = R_H - C_d = R_H' - (C_d - C_m)$ = 47.4 - 2 (C_d = 2 g/l) = 45.4 Percentage of soil remaining in suspension $P = \frac{Ra}{W} \times 100 \%$

(a= 1.015 at 2.57 specific gravity of soil particles and taken as 1.0)

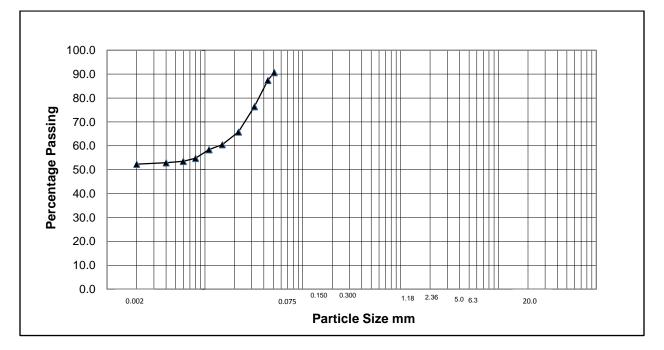
$$= \frac{45.4 \text{ x } 1.0 \text{ x } 100\%}{50}$$

% Finer = 90.7 %

Similarly, from Table A4.1, calculation for % Finer and Diameter of particle can be obtained after 1 min, 2 min, 4 min, 8 min, 15 min, 30 min, 1 hr, 2 hrs and 4 hrs respectively and tabulated below;

Table A4.2:Result	s of Hy	drometer .	Analysis	Test
-------------------	---------	------------	----------	------

Time (min)	$R_{H}^{'}$	$R_{H} = R_{H} + C_{m}$	L (cm)	L/t	D (mm)	$R = R_H - C_d$	% Finer $P = \frac{Ra}{W} \times 100$
0.5	46.9	47.4	8.5	17	0.051	45.4	90.7
1	45.2	45.7	8.8	8.8	0.044	43.7	87.4
2	39.7	40.2	9.7	4.85	0.032	38.2	76.4
4	34.4	34.9	10.6	2.65	0.022	32.9	65.8
8	31.8	32.3	11.1	1.3875	0.015	30.3	60.5
15	30.7	31.2	11.2	0.7467	0.011	29.2	58.4
30	29.9	29.4	11.5	0.3833	0.008	27.4	54.8
60	29.3	28.8	11.9	0.1983	0.006	26.8	53.5
120	29.0	28.5	11.95	0.099583	0.004	26.5	52.9
240	29.2	28.2	12.0	0.05	0.002	26.2	52.3



Finally, Graph of Percentage of Finer vs. Particle Size (Diameter of particle) can be drawn.

Figure A4.1:Graph of Percentage of Finer vs. Particle Size (Diameter of particle)

From above details of hydrometer analysis test, activity of soil(A) can be calculated as follows;

Activity of soil(A) = Plasticity Index / Percent of clay-sized particles (less than $2 \mu m$)

= 18.8 / 52.3

= 0.36

Observations of Standard Proctor Compaction Test

- Mass of the mould = 1.954 kg
- Volume of the mould = $944* 10^{-6} \text{ kg m}^{-3}$

Table A5.1: Standard Proctor	Compaction	Test of	Clayey Sample	÷

NT	Mass of the	Mass of	empty can (g)	Mass of w	vet soil + can (g)
No	mould + soil (g)	Top sample	Bottom sample	Top sample	Bottom sample
1	3.493	9.83	9.17	141.35	165.04
2	3.550	9.54	9.34	142.70	167.45
3	3.648	10.24	9.80	150.80	158.50
4	3.749	10.58	10.50	134.36	140.60
5	3.757	9.56	10.80	144.56	145.70
6	3.751	11.78	9.45	157.80	160.46
7	3.671	10.70	11.96	147.30	150.40

Specimen Calculations of Standard Proctor Compaction Test

For first sample;

Mass of the soil	= (Mass of the mould + soil) – (Mass of the mould)
	= 3.493 kg -1.954 kg
	= 1.539 kg
Bulk density	= (Mass of the soil) / (Volume of the mould)
	$= 1.539 / 944* 10^{-6} \text{ kg m}^{-3}$
	= 1629.98 kg m-3
Moisture content for top sample	= (<u>Mass of the wet soil + can) – (Mass of the dry soil + can)</u> *100 (Mass of the dry soil + can – Mass of the can)
(124.93 – 9.83)	= (<u>141.35 - 124.93)</u> * 100%
	= 14.27 %

Moisture content for bottom sample $= (\underline{165.04 - 145.47}) *100$ (145.47 -9.17) = 14.36%Average moisture content = 14.27 + 14.36= 14.315%Dry density = <u>Bulk density</u> (1 + moisture content) $= \underline{1629.98}$ 1+0.14315 $= 1425.87 \text{ kg m}^{-3}$

Similarly, from Table A5.1, calculation for Dry Density and Moisture Content of other samples can be obtained and tabulated below;

Table A5.2:Dry Density and Moisture Contentof Other Samples

Dry Density(kg m ⁻³)	Moisture Content(%)
1425.87	14.315
1455.10	16.155
1513.62	18.555
1576.71	20.610
1556.45	22.730
1543.55	23.315
1437.24	26.585

Calculation for Dry density at 100% saturation (theoretical) to plot zero air void line can be done using equation - 02;

 $\rho_{d, \max} = \frac{G \rho_{w}}{1 + wG}$ Equation - 02 Where; Specific Gravity (G) = 2.57 Density of Water (P_w) =1000 kg m⁻³ w = Moisture Content For sample 01,

Dry density =
$$\frac{2.57 \text{ x } 1000}{(1 + 0.14315 \text{ x } 2.57)}$$

= 1878.79 kg m⁻³

Similarly values of dry density at 100% saturation can be calculated at different moisture content and tabulated below.

Sample No	Moisture Content (%)	Dry Density (kg m ⁻³)
01	14.315	1878.79
02	16.155	1815.99
03	18.555	1740.13
04	20.610	1680.07
05	22.730	1622.27
06	23.315	1607.05
07	26.585	1526.85

Table A5.3:Dry DensityValuesat 100% Saturation

Observations of Consolidation Test

Table A6.1:Clayey Sample Details

Test method		BS 1377 : Part5 :	1990 :3 Date	30-Oct-16
		Particle density	2.57	Mg/m ³
DIMENSIONS	Initial	Overall	Final	Specimen
	specimen	Change	Specimen	preparation
				method
Diameter D mm	50.00		50.00	
Area A mm ²	1963.50		1963.50	
Height H mm	H _o 20.00	0.000	17.668	
Volume V cm ³	39.27	0.00	39.27	

Table A6.2: Consolidation Test of Clayey Sample

	Settlement Corresponding to the Different Loads							
Time(min)	First Day	Second Day	Third Day	Fourth Day				
	25 kPa	50 kPa	75 kPa	100 kPa				
0	0.000	1.160	1.666	2.020				
0.25	0.212	1.202	1.690	2.040				
0.5	0.236	1.210	1.698	2.044				
1	0.262	1.218	1.712	2.050				
2	0.298	1.232	1.721	2.058				
4	0.360	1.252	1.742	2.068				
8	0.436	1.286	1.764	2.082				
15	0.502	1.328	1.790	2.100				
30	0.626	1.392	1.822	2.128				
60	0.772	1.462	1.858	2.162				
120	0.938	1.532	1.898	2.208				
240	1.052	1.586	1.936	2.240				
1440	1.160	1.666	2.020	2.332				

Specimen Calculations of Consolidation Test

Table A6.3:SpecimensCalculation

WEIGHINGS			Initial spec	imen		Fir	al specimen
			(a)		(b)		(c)
Wet soil + -ring + tray	g		50.80		142.22		67.92
Dry soil + ring + tray	g		38.92		122.85		53.82
Ring + tray	g		19.23		90.73		30.53
Wet soil	g	mo	31.57	mo	51.49		37.39
Dry soil	g	m _d	19.69	m _d	32.12	m _d	23.3
Water	g		11.88		19.37		14.10
Moisture content (measured)	%		60.3		60.3		61.0
Moisture content (from trimmings)	%	Wo			60.3		
Density	Mg/m ³				1.31		0.95
Dry density	Mg/m ³				0.82		0.59
Voids ratio		eo			2.143		3.35
Degree of saturation	%	So			72.4		46.9
Height of solids	H _s mm				6.36		4.07

Table A6.4:Consolidation TestCalculation

		VOIDS RAT	10		COMPRESSIBILITY COEFFICIENT OF CONSOLIDAT				IDATION		
					Incremer	ntal	m _v =		H =	c _v	k
Increment	Pressure	Cumulative	Consolidated	Voids	height	pressure	δН. 1000		1/2(H ₁ +H ₂)	$0.111H^{2}$	$=c_v * m_v * \gamma_w$
No.	Р	Compression	height	ratio	change	change	Η ₁ δρ	t ₉₀		- t ₉₀	
		$(\Delta H-Y)$	H =	e=	δН	бр					*10 ⁻⁷ mm/s
			$Ho-(\Delta H-Y)$	H-H _s	$=H_1-H_2$						(Clay range)
N	kPa			- H _s	mm	kPa	m ² /MN	min	mm	m ² /Year	
0	0	0	20.000	2.143							
L1	25.000	1.160	18.840	1.960	1.160	25.00	2.320	43.560	19.420	0.961	7
L2	50.000	1.666	18.334	1.881	0.506	25.00	1.074	88.360	18.587	0.434	1
L3	75.000	2.020	17.980	1.825	0.354	25.00	0.772	100.000	18.157	0.366	1
L4	100.000	2.332	17.668	1.776	0.312	25.00	0.694	141.610	17.824	0.249	1

According to above calculations, Consolidation test graphs of clayey sample can be drawn as follow.

Consolidation Test Graphs

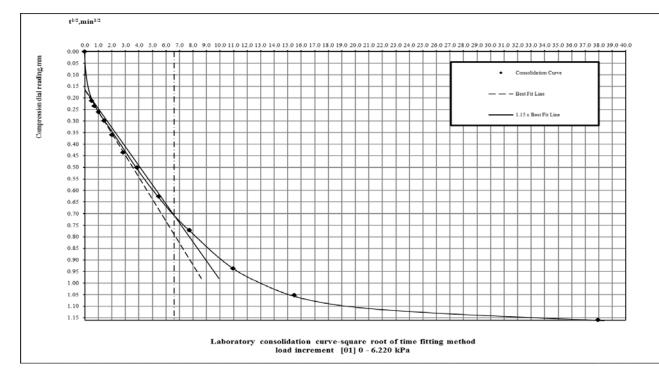


Figure A6.1: Consolidation Graph for 25 kPa Load

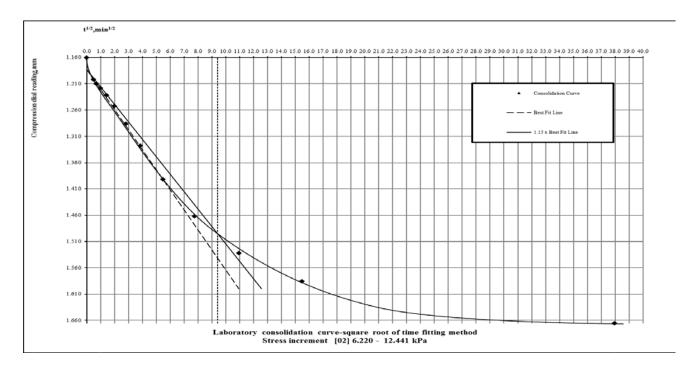


Figure A6.2: Consolidation Graph for 50 kPa Load

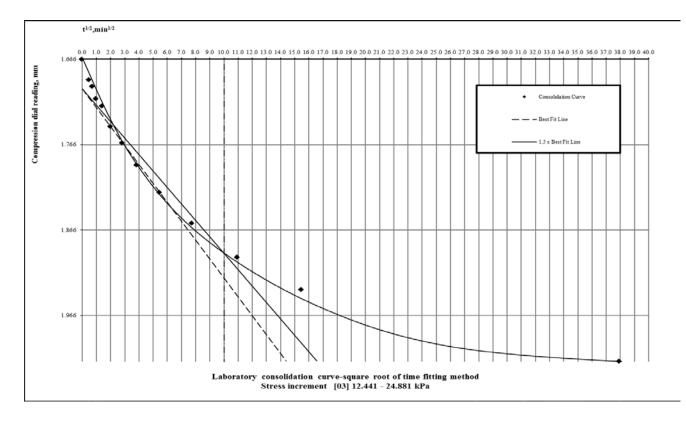


Figure A6.3: Consolidation Graph for 75 kPa Load

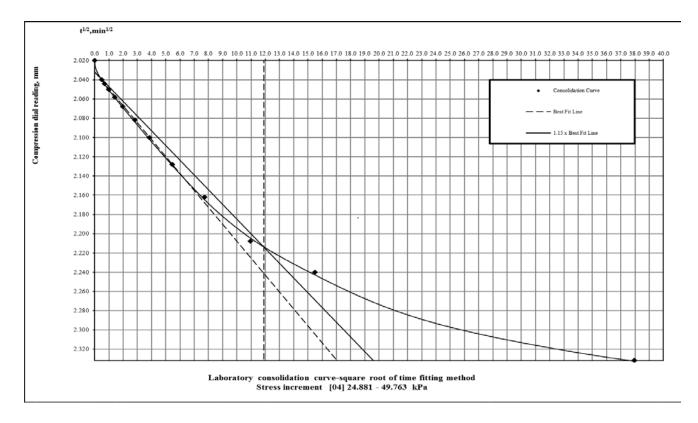


Figure A6.4: Consolidation Graph for 100 kPa Load

Observations of Organic Content Test

- The mass of an empty, clean, and dry porcelain dish $(M_P)(g)=40.32$
- The mass of the dish and soil specimen $(M_{PDS})(g)=49.73$
- The mass of the dish containing the ash (burned soil) $(M_{PA})(g) = 48.60$

Specimen Calculations of Organic Content Test

The mass of the dry soil (M_D)	$= M_{PDS} - M_P$ = 49.73 - 40.32
=9.41g	
The mass of the ashed (burned) soil (M	M_{A}) = $M_{PA} - M_{P}$ = 48.60 - 40.32
= 8.28 g	
The mass of organic matter(M ₀)	$= M_{\rm D} - M_{\rm A}$ = 9.41- 8.28
	= 1.13 g
The organic matter (content) (OM) = 1.13 / 9.41	$= (M_O/M_D)*100$
- 1.15 / 7.41	= 12%

The organic matter (content) of given clayey sample is 12%.

Observations of AIV, ACV and LAAV Tests

Table A8.1: Aggregate Impact Value Test of Concrete Debris

Test No.	1	2
Weight of sample (g)	248.6	248.2
Weight of sample passing 2.36 mm sieve		
after test (g)	78.8	75.2
Weight of sample retained on 2.36 mm sieve		
after test (g)	169.8	173.0

Table A8.2: Aggregate Impact Value Test of Aggregates

Test No.	1	2
Weight of sample (g)	303.4	303.4
Weight of sample passing 2.36 mm sieve		
after test (g)	74.7	77.0
Weight of sample retained on 2.36 mm sieve		
after test (g)	228.4	226.5

Specimen Calculation

From Table A8.1, 2nd set of readings,

Weight of sample in standard measure	= 248.2 g
Weight of sample passing 2.36 mm sieve after test	= 75.2 g
Weight of sample retained on 2.36 mm sieve after test	= 158.3 g
Hence, Aggregate Impact Value of concrete debris	= 30.3 %
Similarly,	
From 1 st set of readings, Aggregate Impact Value	= 31.7 %
Hence, Average Aggregate Impact Value of concrete debris	= 31 %

Note: Plaster debris sample was not be prepared for Aggregate Impact Value Test as it was broken into small particles when preparing sample.

Table A8.3: Aggregate Crushing Value Test of Concrete Debris

Test No.	1	2
Weight of sample in standard measure (g)	2181	2185
Weight of sample passing 2.36 mm sieve		
after test (g)	761	767
Weight of sample retained on 2.36 mm sieve		
after test (g)	1414	1410

Table A8.4: Aggregate Crushing Value Test of Aggregates

Test No.	1	2
Weight of sample in standard measure (g)	2185	2189
Weight of sample passing 2.36 mm sieve		
after test (g)	546	556
Weight of sample retained on 2.36 mm sieve		
after test (g)	1634	1629

Specimen Calculation

From Table A8.3, 2nd set of readings,

Weight of sample in standard measure	= 2185 g
Weight of sample passing 2.36 mm sieve after test	= 767 g
Weight of sample retained on 2.36 mm sieve after test	= 1410 g
Hence, Aggregate Crushing Value of concrete debris	= 767/2185 x 100
	= 35.1 %
Similarly,	
From 1 st set of readings, Aggregate Crushing Value	= 34.9 %

Hence, Average Aggregate Crushing Value of concrete debris = 35 %

Note: Plaster debris sample was not be prepared for Aggregate Crushing Value Test as it broken to small particles when preparing sample

Table A8.5: Los Angeles Abrasive Value Test of Concrete Debris

Test No.	1	2
Total Weight of sample (g)	5000	5000
Weight of sample passing 1.7 mm sieve after		
test (g)	2130	2070
Weight of sample retained on 1.7 mm sieve		
after test (g)	2870	2930

Table A8.6: Los Angeles Abrasive Value Test of Aggregates

Test No.	1	2
Total Weight of sample (g)	5000	5000
Weight of sample passing 1.7 mm sieve after		
test (g)	1596	1544
Weight of sample retained on 1.7 mm sieve		
after test (g)	3400	3449

Specimen Calculation

From Table A8.5, 2nd set of readings,

Total weight of sample (W1 g)	= 5000 g
Weight retained on 1.7 mm sieve after rotation (W2 g)	= 2699 g
Weight passing 1.7 mm sieve after rotation (W2 g)	= 2271 g
Hence, Los Angeles Abrasion Value	= 41.4 %
Similarly,	
From 1 st set of readings, Los Angeles Abrasion Value	= 42.6 %
Hence, Average Los Angeles Abrasion Value of concrete debris	= 42 %

Note: Plaster debris sample was not be prepared for Los Angeles Abrasive Value Test as it broken to small particles when preparing sample.

Observations of Slake Durability Test

Table A9.1: Slake Durability Test of Brick Debris

Test date	Initial	After one month	After two months
Weight of sample, dry weight basis(g)	500	500	500
Weight retained after 1 st cycle, dry weight basis(g)	416	413	412
Weight retained after 2 nd cycle, dry weight basis(g)	357	353	346

Table A9.2: Slake Durability Test of Concrete Debris

Test date	Initial	After one month	After two months
Weight of sample, dry weight basis(g)	500	500	500
Weight retained after 1 st cycle, dry weight basis(g)	479	481	485
Weight retained after 2 nd cycle, dry weight basis(g)	464	470	477

Table A9.3: Slake Durability Test of Plaster Debris

Test date	Initial	After one month	After two months
Weight of sample, dry weight basis(g)	500	500	500
Weight retained after 1 st cycle, dry weight basis(g)	460	481	479
Weight retained after 2 nd cycle, dry weight basis(g)	459	465	467

Specimen Calculations of Slake Durability Test

From Table A9.1, Initial set of readings;	
Weight of sample, dry weight basis (g)	= 500 g
Weight retained after 1 st cycle, dry weight basis (g)	= 416 g
Hence, Slake Indexof Brick debris after 1 st cycle	=(416/500)x100 %
	= 83.2 %
Weight retained after 2 nd cycle, dry weight basis (g)	= 357 g
Hence, Slake Index of Brick debris after 2 nd cycle	$= (357/500) \times 100\%$
=71.4 %	
Similarly;	
From after one month set of readings,	
Slake Index of Brick debrisafter 1 st cycle=82.6 % Slake Index of Brick debris after 2 nd cycle =	70.6 %
From after two months set of readings,	
Slake Index of Brick debrisafter 1^{st} cycle= 82.4 % Slake Index of Brick debris after 2^{nd} cycle =	69.2 %

Similarly, calculation was done for concrete block debris and cement plaster separately and values are tabulated below;

Table A9.4: Initial Values of Slake Durability Test of Different Type of Debris

Sample name	Initial weight,dry weight basis (g)	Weight retained after 1 st cycle, dry weight basis (g)	% Weight retained after 1 st cycle, dry weight basis	Weight retained after 2 nd cycle, dry weight basis (g)	% Weight retained after 2 nd cycle, dry weight basis
Concrete	500	479	95.8	464	92.8
Plaster	500	460	92.0	459	91.8
Brick	500	416	83.2	357	71.4

Sample name	Initial weight,dry weight basis (g)	Weight retained after 1 st cycle, dry weight basis (g)	% Weight retained after 1 st cycle, dry weight basis	Weight retained after 2 nd cycle, dry weight basis (g)	% Weight retained after 2 nd cycle, dry weight basis
Concrete	500	481	96.2	470	94.0
Plaster	500	481	96.2	465	93.0
Brick	500	413	82.6	353	70.6

Table A9.5: Values of Slake Durability Test of Different Type of Debris after One Month

Table A9.6: Values of Slake Durability Test of Different Type of Debrisafter Two Months

Sample name	Initial weight,dry weight basis (g)	Weight retained after 1 st cycle, dry weight basis (g)	% Weight retained after 1 st cycle, dry weight basis	Weight retained after 2 nd cycle, dry weight basis (g)	% Weight retained after 2 nd cycle, dry weight basis
Concrete	500	485	97.0	477	95.4
Plaster	500	479	95.8	467	93.4
Brick	500	412	82.4	346	69.2

These values can be shown graphically in Figure A9.1, Figure A9.2 and Figure A9.3.

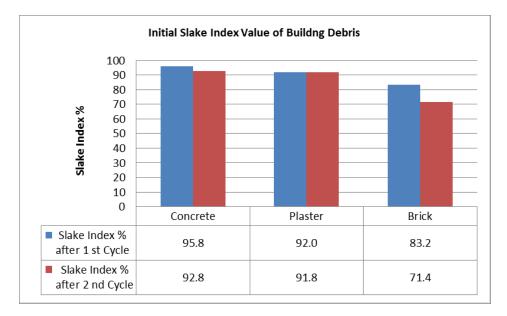


Figure A9.1:Initial Slake Index Values of Different Type of Debris

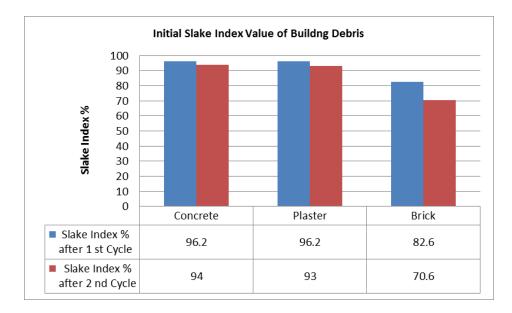


Figure A9.2:Slake Index Values of Different Type of Debris after One Month

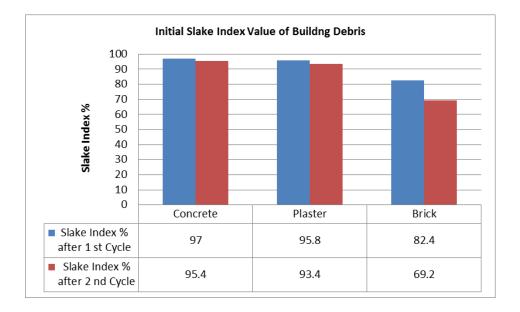


Figure A9.3:Slake Index Values of Different Type of Debris after Two Months

Observations of Compressive Strength Test

Table A10.1:Compressive Strength Test of Concrete

Penetration of Plunger (cm)	Dial Reading of proving ring
0	0
0.125	1
0.25	2
0.375	2
0.5	3
0.625	3
0.75	3
0.875	3
1	4
1.125	4
1.25	4
1.375	4
1.5	4
1.625	4
1.75	5
1.875	5 5
2	5
2.125	5 5 5
2.25	5
2.375	5 5 5
2.5	5
2.625	5

2.875	6
3	6
3.125	6
3.25	6
3.375	6
3.5	7
3.625	7
3.75	7 7
3.875	7
4	7
4.125	7
4.25	8
4.375	8
4.5	8
4.625	8
4.75	8
4.875	9
5	9
5.125	9
5.25	9
5.375	10
5.5	10
5.625	10
5.75	10
5.875	10
6	10

Dial Reading of proving ring
0
1
1
2
3
4
5
6
6
6
7
7
7
7 7
7
8
8
8
8
8
8
9
9

2.875	9
3	9
3.125	9
3.25	10
3.375	10
3.5	10
3.625	10
3.75	10
3.875	10
4	11
4.125	11
4.25	11
4.375	11
4.5	11
4.625	12
4.75	12
4.875	12
5	12
5.125	12
5.25	12
5.375	12
5.5	13
5.625	13
5.75	13
5.875	13
6	13

	1
Penetration of Plunger	Dial Reading of proving ring
(cm)	
0	0
0.125	1
0.25	1
0.375	1
0.5	1
0.625	1
0.75	1
0.875	1
1	1
1.125	1
1.25	1
1.375	1
1.5	1
1.625	1
1.75	2
1.875	2
2	2
2.125	2
2.25	2
2.375	2
2.5	2
2.625	2
2.75	2
2.125 2.25 2.375 2.5 2.625	2 2 2 2 2 2 2 2 2 2 2

2.875	2
3	2
3.125	
3.25	2 3
3.375	3
3.5	3
3.625	3
3.75	3
3.875	3
4	3
4.125	3
4.25	3
4.375	3
4.5	3
4.625	3
4.75	3
4.875	4
5	4
5.125	4
5.25	4
5.375	4
5.5	4
5.625	4
5.75	4
5.875	4
6	4

Dial Reading of proving ring
0
1
1
1
2
2 2 2 3 3 3 3 3
2
3
3
3
3
3
3
3
4
4
4
4
4
4
4
4
5

2.875	5
3	5
3.125	5
3.25	5
3.375	5
3.5	5
3.625	5
3.75	5
3.875	5
4	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
4.125	5
4.25	5
4.375	5
4.5	5
4.625	6
4.75	6
4.875	6
5	6
5.125	6
5.25	6
5.375	6
5.5	6
5.625	6
5.75	6
5.875	6
6	6

	r
Penetration	Dial Reading
of Plunger	of proving ring
(cm)	Ing
0	0
0.125	1
0.125	2
0.25	2
0.5	2 3
0.625	3
0.75	3
0.875	3
1	4
1.125	4
1.25	4
1.375	4
1.5	4
1.625	4
1.75	5
1.875	5 5 5
2	
2.125	5
2.25	6
2.375	6
2.5	6
2.625	6
2.75	6
2.875	6

3	6
3.125	7
3.25	7
3.375	7
3.5	7
3.625	7
3.75	7
3.875	8
4	8
4.125	8
4.25	8
4.375	8
4.5	8
4.625	8
4.75	8
4.875	9
5	9
5.125	9
5.25	9
5.375	9
5.5	9
5.625	9
5.75	10
5.875	10
6	10
P	

Values of Compressive Strength Test

Table A11.1: Compressive Strength Values of Concrete

Penetration	Dial Reading	Actual	
of Plunger	of proving	Load	
	ring		
(cm)		(kN)	
0	0	0.03	
0.125	1	0.05	
0.25	2	0.07	
0.375	2	0.07	
0.5	3	0.09	
0.625	3	0.09	
0.75	3	0.09	
0.875	3	0.09	
1	4	0.11	
1.125	4	0.11	
1.25	4	0.11	
1.375	4	0.11	
1.5	4	0.11	
1.625	4	0.11	
1.75	5	0.13	
1.875	5	0.13	
2	5	0.13	
2.125	5	0.13	
2.25	5	0.13	
2.375	5	0.13	
2.5	5	0.13	
2.625	5	0.13	

2.875	6	0.15
3	6	0.15
3.125	6	0.15
3.25	6	0.15
3.375	6	0.15
3.5	7	0.17
3.625	7	0.17
3.75	7	0.17
3.875	7	0.17
4	7	0.17
4.125	7	0.17
4.25	8	0.19
4.375	8	0.19
4.5	8	0.19
4.625	8	0.19
4.75	8	0.19
4.875	9	0.21
5	9	0.21
5.125	9	0.21
5.25	9	0.21
5.375	10	0.23
5.5	10	0.23
5.625	10	0.23
5.75	10	0.23
5.875	10	0.23
6	10	0.23

Penetration of Plunger	Dial Reading of proving ring	Actual Load	
(cm)	0	KN	
0	0	0.03	
0.125	1	0.05	
0.25	1	0.05	
0.375	2	0.07	
0.5	3	0.09	
0.625	4	0.11	
0.75	5	0.13	
0.875	6	0.15	
1	6	0.15	
1.125	6	0.15	
1.25	7	0.17	
1.375	7	0.17	
1.5	7	0.17	
1.625	7	0.17	
1.75	7	0.17	
1.875	8	0.19	
2	8	0.19	
2.125	8	0.19	
2.25	8	0.19	
2.375	8	0.19	
2.5	8	0.19	
2.625	9	0.21	
2.75	9	0.21	

9	0.21
9	0.21
9	0.21
10	0.23
10	0.23
10	0.23
10	0.23
10	0.23
10	0.23
11	0.25
11	0.25
11	0.25
11	0.25
11	0.25
12	0.27
12	0.27
12	0.27
12	0.27
12	0.27
12	0.27
12	0.27
13	0.29
13	0.29
13	0.29
13	0.29
13	0.29
	9 9 10 10 10 10 10 10 10 10 10 11 11 11 11 11 12 12 12 12 12 12 12 12 12 13 13 13

	Dial Deading		
Penetration	Dial Reading	Actual	
of Plunger	of proving ring	Load	
(cm)	Ing	KN	
0	0	0.03	
0.125	1	0.05	
0.25	1	0.05	
0.375	1	0.05	
0.5	1	0.05	
0.625	1	0.05	
0.75	1	0.05	
0.875	1	0.05	
1	1	0.05	
1.125	1	0.05	
1.25	1	0.05	
1.375	1	0.05	
1.5	1	0.05	
1.625	1	0.05	
1.75	2	0.07	
1.875	2	0.07	
2	2	0.07	
2.125	2	0.07	
2.25	2	0.07	
2.375	2	0.07	
2.5	2	0.07	
2.625	2	0.07	
2.75	2	0.07	

2.875	2	0.07
3	2	0.07
3.125	2	0.07
3.25	3	0.09
3.375	3	0.09
3.5	3	0.09
3.625	3	0.09
3.75	3	0.09
3.875	3	0.09
4	3	0.09
4.125	3	0.09
4.25	3	0.09
4.375	3	0.09
4.5	3	0.09
4.625	3	0.09
4.75	3	0.09
4.875	4	0.11
5	4	0.11
5.125	4	0.11
5.25	4	0.11
5.375	4	0.11
5.5	4	0.11
5.625	4	0.11
5.75	4	0.11
5.875	4	0.11
6	4	0.11

Derret	Dial Reading	A at1
Penetration of Plunger	of proving	Actual Load
(cm)	ring	KN
0	0	0.03
0.125	1	0.05
0.25	1	0.05
0.375	1	0.05
0.5	2	0.07
0.625	2	0.07
0.75	2	0.07
0.875	3	0.09
1	3	0.09
1.125	3	0.09
1.25	3	0.09
1.375	3	0.09
1.5	3	0.09
1.625	3	0.09
1.75	4	0.11
1.875	4	0.11
2	4	0.11
2.125	4	0.11
2.25	4	0.11
2.375	4	0.11
2.5	4	0.11
2.625	4	0.11
2.75	5	0.13

2.875	5	0.13
3	5	0.13
3.125	5	0.13
3.25	5	0.13
3.375	5	0.13
3.5	5	0.13
3.625	5	0.13
3.75	5	0.13
3.875	5	0.13
4	5	0.13
4.125	5	0.13
4.25	5	0.13
4.375	5	0.13
4.5	5	0.13
4.625	6	0.15
4.75	6	0.15
4.875	6	0.15
5	6	0.15
5.125	6	0.15
5.25	6	0.15
5.375	6	0.15
5.5	6	0.15
5.625	6	0.15
5.75	6	0.15
5.875	6	0.15
6	6	0.15

Penetration of Plunger	Dial Reading of proving ring	Actual Load	
(cm)		KN	
0	0	0.03	
0.125	1	0.05	
0.25	2	0.07	
0.375	2	0.07	
0.5	3	0.09	
0.625	3	0.09	
0.75	3	0.09	
0.875	3	0.09	
1	4	0.11	
1.125	4	0.11	
1.25	4	0.11	
1.375	4	0.11	
1.5	4	0.11	
1.625	4	0.11	
1.75	5	0.13	
1.875	5	0.13	
2	5	0.13	
2.125	5	0.13	
2.25	6	0.15	
2.375	6	0.15	
2.5	6 0.15		
2.625	6	0.15	
2.75	6	0.15	
2.875	6	0.15	

3	6	0.15
3.125	7	0.17
3.25	7	0.17
3.375	7	0.17
3.5	7	0.17
3.625	7	0.17
3.75	7	0.17
3.875	8	0.19
4	8	0.19
4.125	8	0.19
4.25	8	0.19
4.375	8	0.19
4.5	8	0.19
4.625	8	0.19
4.75	8	0.19
4.875	9	0.21
5	9	0.21
5.125	9	0.21
5.25	9	0.21
5.375	9	0.21
5.5	9	0.21
5.625	9	0.21
5.75	10	0.23
5.875	10	0.23
6	10	0.23

Observations of Vane Shear Test

	Test Depth	Shear Strength(divisions) fromApparatus for Clay Surrounding			r Clay	
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
80 mm from center of model	0	20	20	21	19	7.5
80 mm from center of model	80	26	24	23	22	11

Table A12.1: Vane Shear Test at 80 mm Distancefrom Center of Model Initially

Table A12.2: Vane Shear Test at 35 mm Distancefrom Center of Model Initially

	Test Depth	Shear Strength(divisions) fromApparatus for Clay Surrounding					
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay	
35 mm from center of model	0	24	24	24	23.5	12	
35 mm from center of model	80	32	30	31	29	16	

Table A12.3:Vane Shear Test at 80 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

	Test Depth	Shear Strength(divisions) fromApparatus for Clay Surrounding				
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
80 mm from center of model	0	26	21	22	20	10
80 mm from center of model	80	36	32	34	34	13

Table A12.4:Vane Shear Test at 35 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

	Test Depth	Shear Strength(divisions) fromApparatus for Clay Surrounding				
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
35 mm from center of model	0	34	31	30	32	14
35 mm from center of model	80	40	39	37	38	22

Table A12.5:Vane Shear Test at 80 mm Distancefrom Center of Model with Load after One Month Soaked Period

	Test Depth	Surrounding					
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay	
80 mm from center of model	0	31	30	29	29	13	
80 mm from center of model	80	42	37	36	36	17	

Table A12.6:Vane Shear Test at 35 mm Distancefrom Center of Model with Load after One Month Soaked Period

	Test Depth	Shear Strength(divisions) fromApparatus for Clay Surrounding				
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
35 mm from center of model	0	37	36	34	36	17
35 mm from center of model	80	45	43	39	42	24

Shear Strength Values of Clay Surrounding

	Test Depth	Shear	Strength(kPa) of Clay	lay Surrounding			
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay		
80 mm from center of model	0	6	6	6	5	2		
80 mm from center of model	80	7	7	6	6	3		

Table A13.1:Shear Strength Valuesat 80 mm Distancefrom Center of Model Initially

Table A13.2:Shear Strength	Valuesat 35 mm	Distancefrom	Center of Model Initially

	Test Depth	Shear Strength(kPa) of Clay Surrounding				ng
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
35 mm from center of model	0	7	7	7	6.5	3
35 mm from center of model	80	9	8	9	8	4

Table A13.3:Shear Strength Valuesat 80 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

	Test Depth	Shear Strength(kPa) of Clay Surrounding with load(8 kg) after 07 days				th load(8
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
20 mm from edge of model	0	7	6	6	6	3
20 mm from edge of model	80	10	9	9	9	4

Table A13.4:Shear Strength Valuesat 35 mm Distancefrom Center of Model with Load after 07 Days Soaked Period

	Test Depth	Shear Strength(kPa) of Clay Surrounding with load(8 kg) after 07 days				
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
35 mm from center of model	0	9	9	8	9	4
35 mm from center of model	80	11	11	10	11	6

Table A13.5:Shear Strength Valuesat 80 mm Distancefrom Center of Model with Load after One Month Soaked Period

	Test Depth	Shear Strength(kPa) of Clay Surrounding with load(8 kg) after One Month				
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
20 mm from edge of model	0	9	8	8	8	4
20 mm from edge of model	80	12	10	10	10	5

Table A13.6:Shear Strength Valuesat 35 mm Distancefrom Center of Model with Load after One Month Soaked Period

	Test Depth	Shear Strength(kPa) of Clay Surrounding with load(8 kg) after One Month				
Test Location	(mm)	Aggregate	Concrete	Plaster	Brick	Clay
35 mm from center of model	0	10	10	9	10	5
35 mm from center of model	80	13	12	11	12	7

Table A14.1: Shear Strength Calibration Chart for the 33 mm Blade

Divisions	kPa	Divisions	kPa	Divisions	kPa	Divisions	kPa
1	0	36	10	71	20	106	30
2	1	37	10	72	20	107	30
3	1	38	11	73	20	108	30
4	1	39	11	74	21	109	30
5	1	40	11	75	21	110	31
6	2	41	11	76	21	111	31
7	2	42	12	77	21	112	31
3	2	43	12	78	22	113	31
9 •	3	44	12	79	22	114	32
10	3	45	13	80	22	115	32
11	3	46	13	81	23	116	32
12	3	47	13	82	23	117	33
13	4	48	13	83	23	118	33
14	4	49	14	84	23	119	33
15	4	50	14	85	24	120	33
16	4	51	14	86	24	121	34
17	5	52	14	87	24	122	34
18	5	53	15	88	25	123	34
19	5	54	15	89	25	124	35
20	6	55	15	90	25	125	35
21	6	56	16	91	25	126	35
22	6	57	16	92	26	127	35
	6	58	16	93	26	128	36
23 24	7	59	16	94	26	129	36
	7	60	17	95	26	130	36
25	7	61	17	96	27	131	36
26		62	17	97	27	132	37
27	8	63	18	98	27	133	37
28	8		18	99	28	134	37
29	8	64	18	100	28	135	38
30	8	65	18	101	28	136	38
31	9	66	19	102	28	137	38
32	9	67		102	29	138	38
33	9	68	19	104	29	139	39
34	9	69	19	104	29	140	39
35	10	70	20	105	20		



Figure A15.1: Construction Debris



Figure A15.2: Concrete Debris



Figure A15.3: Brick Debris



Figure A15.4: Cement Plaster Debris